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**ORIGINAL**

## Pilot Evaluation of Sailplane Handling Qualities

A. G. Bennett, Jr.

GRANT NSG-1284  
MAY 1978

**NASA**

NASA Contractor Report 2960

## Pilot Evaluation of Sailplane Handling Qualities

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Prepared for  
Langley Research Center  
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National Aeronautics  
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## 1. INTRODUCTION

The performance of competition sailplanes as measured by maximum lift to drag ratio ( $L/D_{\max}$ ) or average cross-country speed has shown a steady improvement with time as shown in Figure 1 (Reference 1). This performance improvement has been due to the continual evolution of airfoils and of fiberglass and metal structures to achieve low drag and high aspect ratio wings. The quest for high performance has had a profound effect upon the handling qualities of sailplanes. The increased  $L/D_{\max}$  has increased the range of flight speeds. To minimize the trim drag, the static stability margin has been decreased which has increased control sensitivity and decreased pitch control force gradients. The very slender wing and fuselage structures have also introduced aeroelastic effects upon the sailplane control response characteristics.

There has been some concern voiced about the trends in high performance sailplane handling qualities. Poor handling qualities generally result in increased pilot workload which may compromise flight safety. Thus there is a strong interest in determining whether the current trends in sailplane performance improvement can continue while at the same time a high level of flight safety can be maintained.

The primary objective of this study was to make a qualitative evaluation of all aspects of high performance sailplane handling qualities and to define areas which require further study. To accomplish this objective at a modest cost, a round-robin flight evaluation of several sailplanes by several test pilots was conducted. The Cooper-Harper Rating Scale and pilots' comments

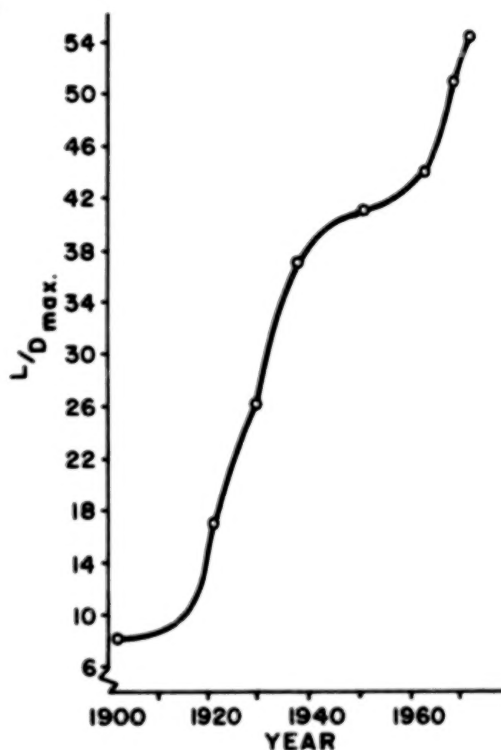


Figure 1.  $L/D_{\max}$  Versus Time

were to be used to evaluate the sailplane handling qualities. The specific objectives of this study were:

1. Using the Cooper-Harper Rating Scale and pilot comments investigate the handling qualities of high performance sailplanes.
2. Obtain pilot opinion of handling quality characteristics to assist the formulation of airworthiness standards.
3. Develop a data base of pilot opinion which would be of value in the design of future sailplanes.
4. Delineate areas which warrant more quantitative study.

The development of high performance sailplanes has evolved in discrete stages with several sailplanes vying for the market at each stage. Thus it was determined that if the sailplanes developed since the early 60's were arranged into groups, then one sailplane from each group should be chosen for the evaluation session. The sailplane grouping logic is given as follows:

- Group 1: Borderline between utility and racing class,  $L/D_{max}$  mid 30's.
- Group 2: First sailplanes to use fiberglass structures. Represents technology in the late 60's. Most have camber changing flaps and/or drag chute.
- Group 3: Sailplanes developed in early 70's. Most numerous class in USA today, hence important.
- Group 4: Sailplanes developed during mid 70's. Just becoming available in substantial numbers. Most have landing flaps.
- Group 5: Very high performance,  $L/D_{max} = 50$ . Effect of large span on handling can be established by this class.
- Group 6: High performance two place. Used in transition to high performance single place sailplanes.

Test pilots for the flight session were chosen from NASA, FAA and the soaring community to ensure that a wide range of pilot backgrounds would be brought to bear upon the sailplane handling quality evaluations.

The text which follows describes the evaluation session and presents the analysis of the pilot opinion data. Chapter 2 describes the sailplanes, pilots and the flight session. Chapter 3 presents the analysis of the pilot

ratings and comments. The evaluation questionnaire, pilot ratings, and pilot comments are presented in the Appendices.

The sailplane owners are due a special thanks for lending their sailplanes for the flight test session. They were Mr. John Thompson, McCrory, Arkansas; Mr. Lanier Franz, Roanoke, Virginia; Mr. Dave Lawrence, Starkville, Mississippi; Mr. Marion Griffith, Dallas, Texas; Schweizer Aircraft Corporation, Elmira, New York; and the Air Force Flight Dynamics Laboratory, Dayton, Ohio. Many members of the Soaring Society of America gave this project unstinting support. Mr. Howard Ebersole, Associate Director of the RASPET Flight Research Laboratory, provided excellent organizational support in the sailplane preparation and in the flight session. The departmental staff support for this project was as usual, superb.

## 2. SAILPLANE FLIGHT TEST SESSION DESCRIPTION

### 2.1 Introduction

The flight test session had to satisfy several requirements and constraints. The round-robin evaluation format required that six sailplanes and seven test pilots must be on site simultaneously. To accommodate the pilots busy flight schedules, the flight session was organized to conduct the flight activities necessary to acquire the required data in a maximum of 7 days. The session was scheduled for the early May period to avoid conflicts with the soaring season, and yet to have the possibility of encountering soaring conditions. In all respects, the flight session was a complete success. There were no problems acquiring the sailplanes, the weather during the flight session was perfect, the test pilots were very enthusiastic, and cooperative, and all operations were conducted safely.

### 2.2 Evaluation Sailplanes

Within the previously mentioned groups of sailplanes, a rating was made to determine which one had characteristics of most interest to this investigation. At the same time, only sailplanes with standard approved type certificates were considered. The soaring community was most cooperative in supporting the acquisition of the evaluation sailplanes.

Sailplane 1. This sailplane was chosen since it represents the transition to higher performance ships. It has a fixed horizontal stabilizer with a fairly large chord elevator. The fixed gear is ahead of the center of gravity. The sailplane is equipped with Schempp-Hirth type divebrakes.

Sailplane 2. This sailplane is equipped with camber changing flaps which are inter-connected with the ailerons. The landing gear is retractable and is ahead of the center of gravity. The sailplane has Schempp-Hirth type divebrakes, and a very short, straight control stick. The sailplane is placarded against intentional spins.

Sailplane 3. This sailplane was selected from Group 3. It has an all-moveable horizontal tail and a control stick which curves slightly toward the pilot. The ship is equipped with retractable landing gear ahead of the center

Table 1  
Sailplane Dimensional Parameters

Parameters	Units	Sailplane					
		1	2	3	4	5	6
Wing Span	m	15.0	15.0	15.0	15.0	20.3	17.4
Wing Area	m <sup>2</sup>	12.40	9.40	10.00	9.64	14.40	16.72
Aspect Ratio		18.1	23.6	22.5	23.3	28.6	18.0
MAC	m	0.885	0.687	0.704	0.681	0.756	1.069
Max Weight	kg	299	300	300/390	299/422	445/580	649
Wing Loading	n/m <sup>2</sup>	234.6	311.2	325.6/383	306.4/430.9	301.6/392.6	378.3
Root Chord	m	1.232	0.940	0.955	0.914	0.980	1.483
Tip Chord	m	0.394	0.343	0.368	0.373	0.350	0.483
Fuselage Length	m	6.680	6.198	6.350	5.842	7.290	8.153
Fuselage Width	m	0.584	0.610	0.635	0.586	0.610	0.813
Hor. Tail Area	m <sup>2</sup>	1.65	1.04	0.99	1.00	0.99	2.03
Hor. Tail Span	m	2.819	2.395	2.408	2.032	2.408	3.200
Elevator $c_{\ell}/c$		0.42	0.28	1.00	0.56	1.00	1.00
Vert. Tail Area	m <sup>2</sup>	1.13	1.06	0.84	0.78	---	1.43
L/D max (Handbook)		32	39	35.2	37	49	34
Fwd C.G.	$\bar{x}$	20	25	26	27.8	29	25
Aft C.G.	$\bar{x}$	40	52	47	38.2	45	38
$I_{yy}$ (Approx.)	kg m <sup>2</sup>	186	186	204	186	407	1178

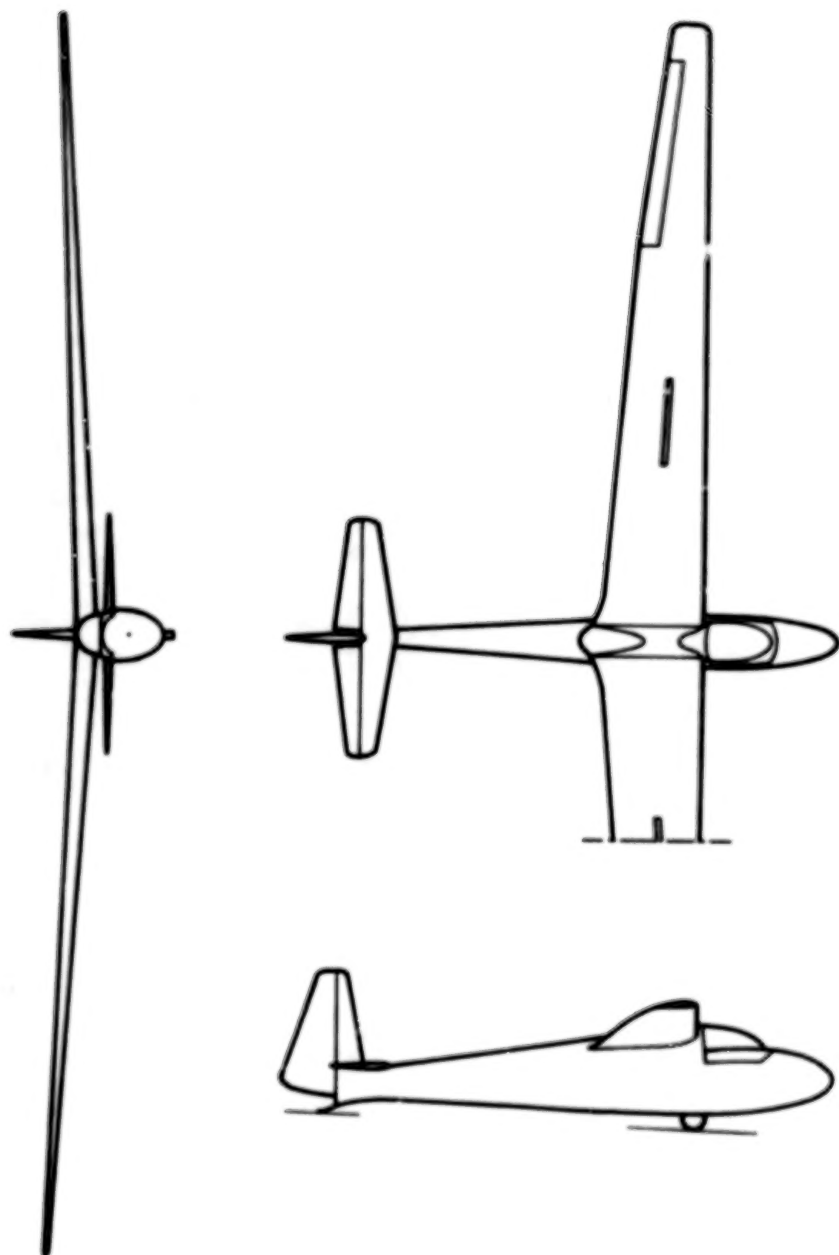


Figure 2. Three View of Sailplane 1.

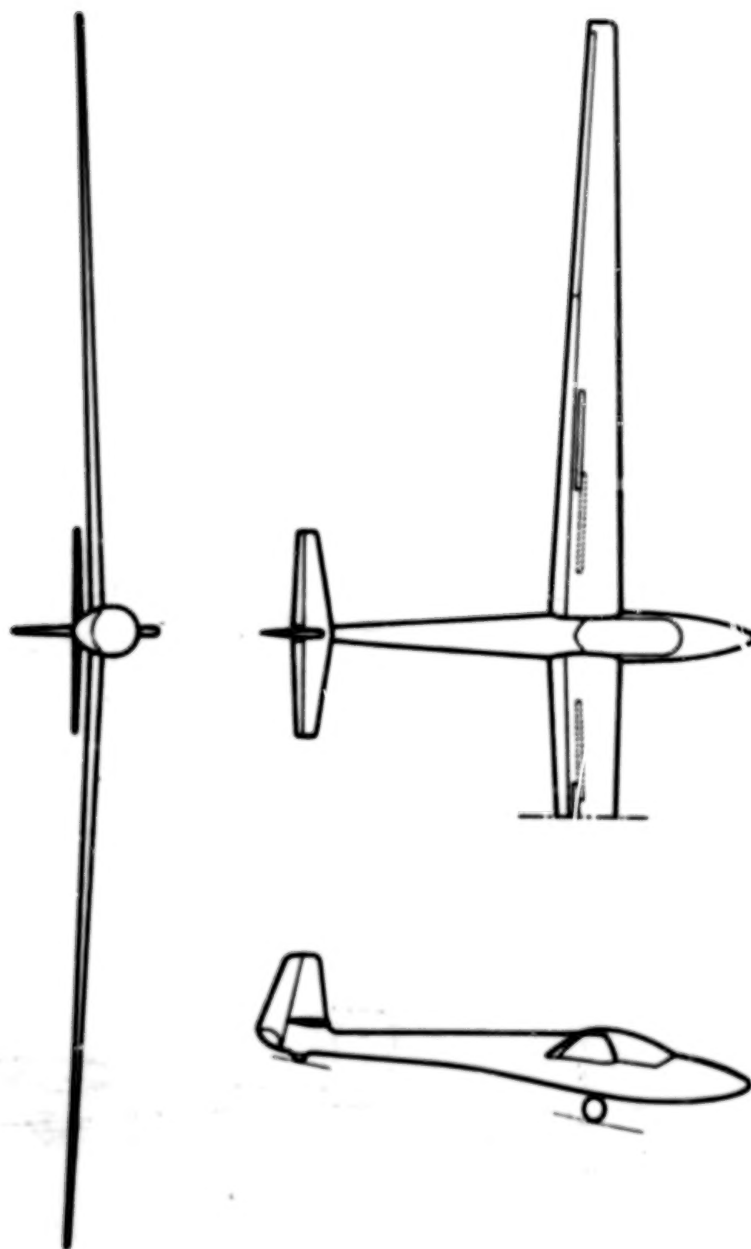


Figure 3. Three View of Sailplane 2.



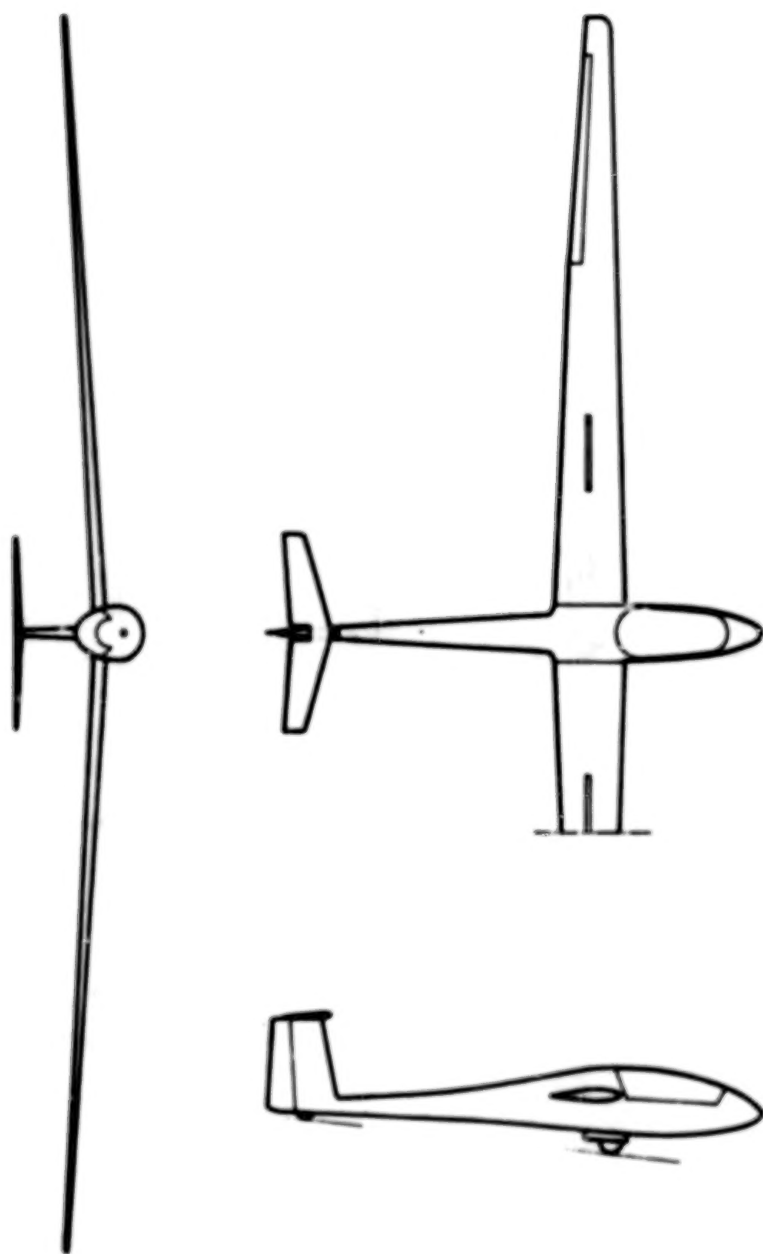


Figure 4. Three View of Sailplane 3.

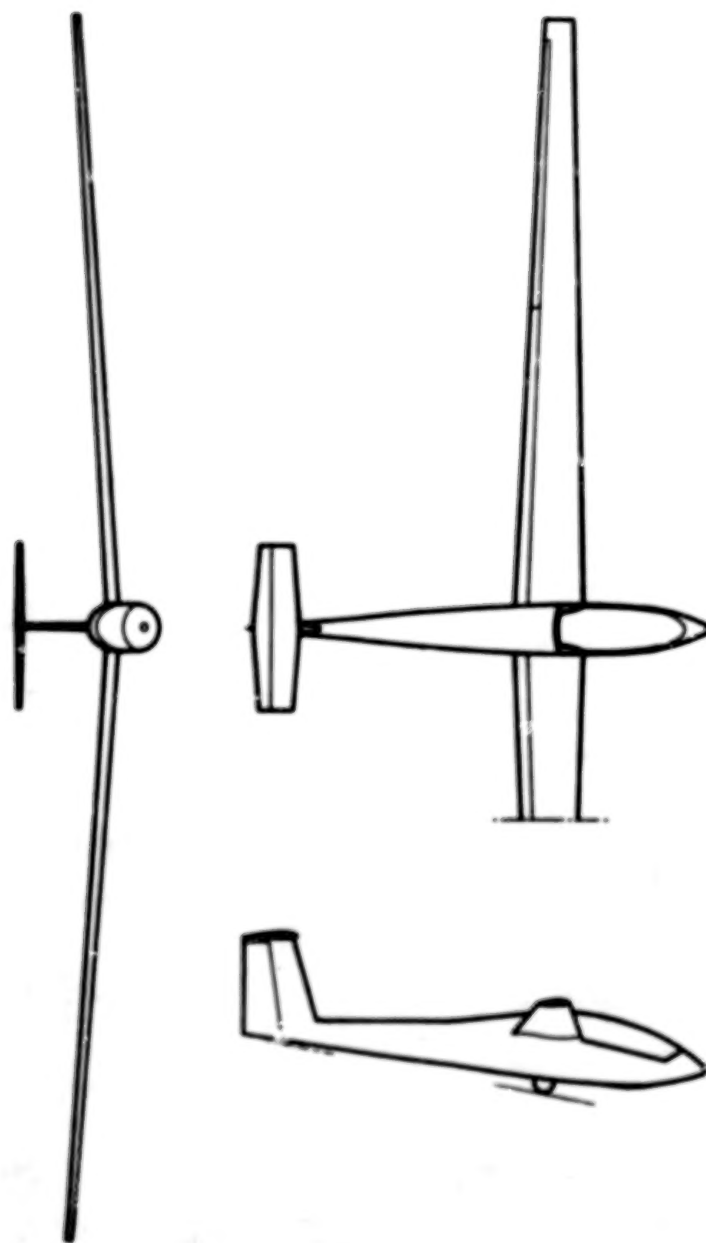


Figure 5. Three View of Sailplane 4.

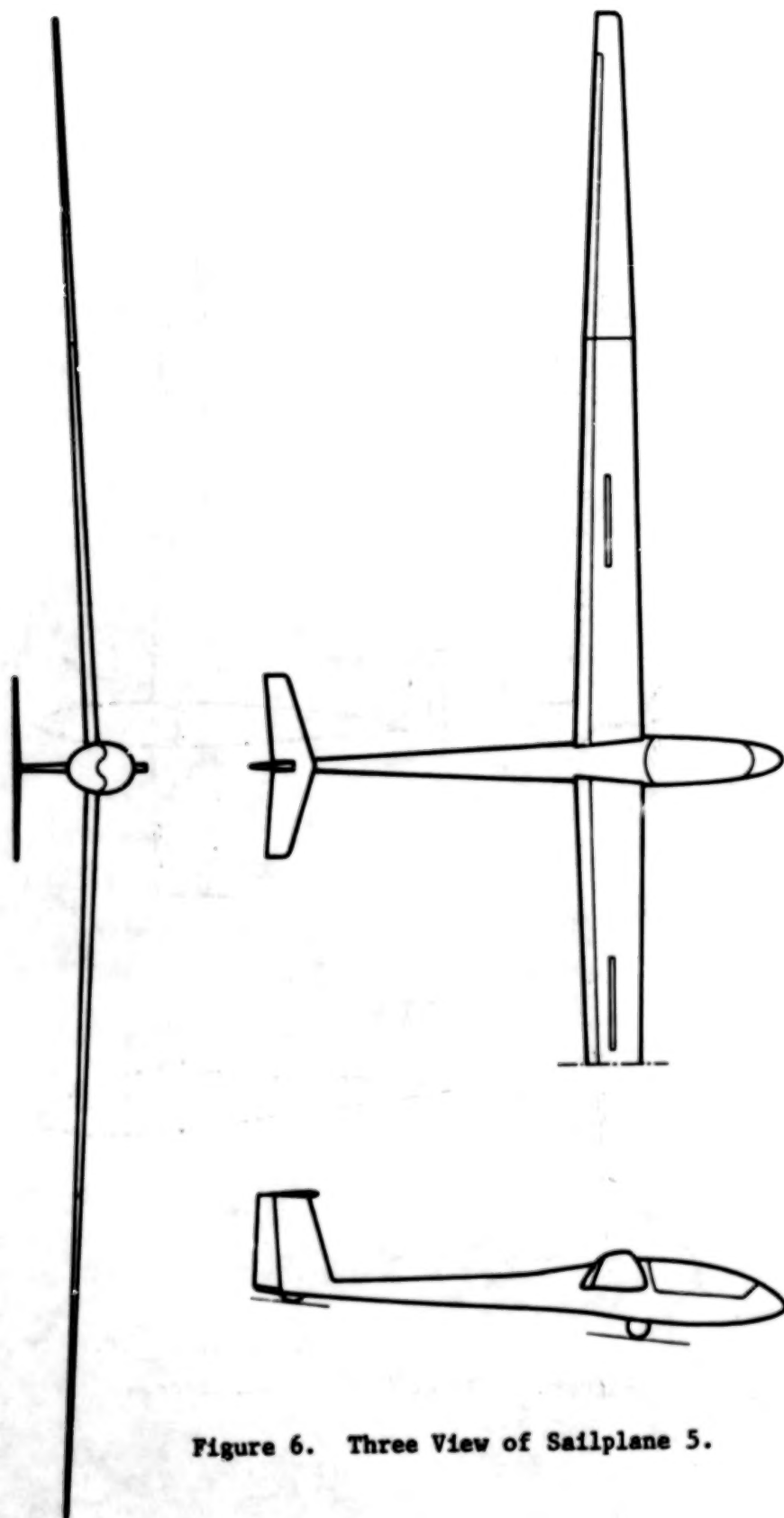


Figure 6. Three View of Sailplane 5.

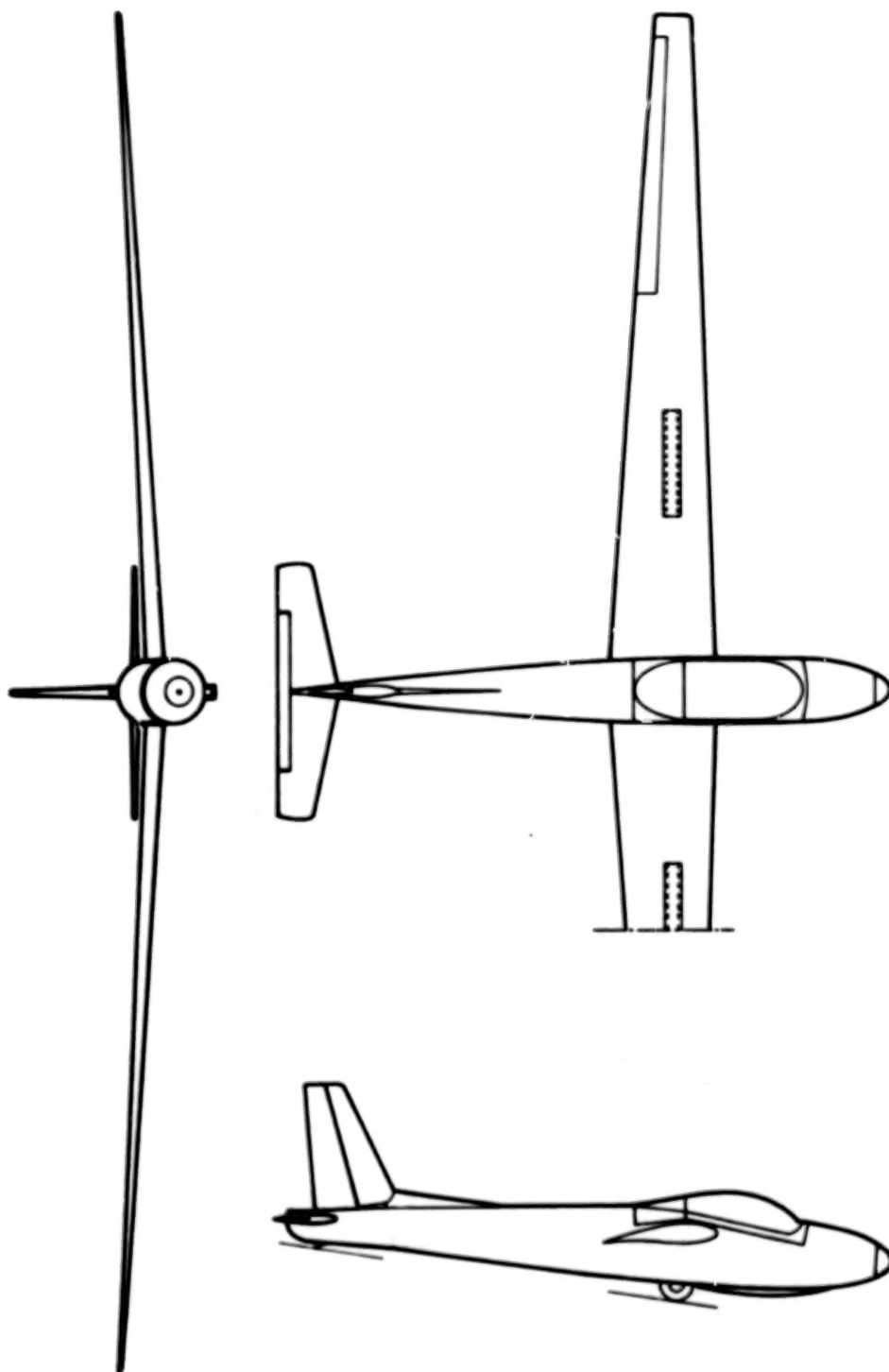


Figure 7. Three View of Sailplane 6.

of gravity, and has upper surface divebrakes. Intentional spins are prohibited with this sailplane.

Sailplane 4. This sailplane has a conventional fixed stabilizer and moveable elevator. The retractable landing gear is located slightly behind the center of gravity. The camber changing flaps, interconnected with the ailerons, can be positioned up to 90 degrees for landing.

Sailplane 5. This ship had the largest wing span among the evaluation sailplanes. The horizontal tail, control stick and landing gear arrangement was identical to that of sailplane 3. This ship is equipped with camber changing flaps interconnected with the ailerons, and with upper surface divebrakes.

Sailplane 6. This sailplane represented a typical, fairly high performance two seater. It features a fixed landing gear, an all moveable horizontal tail equipped with anti-servo tab and large counterbalanced dive brakes.

A three-view drawing of each sailplane is shown in Figures 2 through 7, and the principal geometric characteristics are presented in Table 1.

In general, each sailplane was in excellent mechanical condition. Since in some of the ships intentional spins were prohibited and/or some of the ships were not equipped with water ballast or drag chutes, the effect of these three-factors on the overall sailplane handling qualities was not evaluated.

### 2.3 Evaluation Pilots

Each evaluation pilot is affiliated with one of the following organizations: Soaring Society of America, Inc., the Federal Aviation Administration and the National Aeronautics and Space Administration. Table 2 indicates the number of flight hours as pilot in command of each pilot. Two of the pilots were professional experimental test pilots and had considerable experience with the Cooper-Harper rating scale. Four of the seven pilots had considerable sailplane cross-country and competition flying experience. Preceding the flight test sessions, these four pilots were asked to describe to the rest of the group in detail what they conceive to be the flight role or mission of

a high-performance sailplane. Thus, all of the pilots had a clear understanding of the broad mission for which this class of aircraft is designed.

Table 2  
Evaluation Pilot Flight Experience

<u>Aircraft Type</u>	<u>Pilot</u>						
	<u>1</u>	<u>2</u>	<u>3</u>	<u>4</u>	<u>5</u>	<u>6</u>	<u>7</u>
Sailplane	6500	1500	700	30	20	1500	20
SEL	500	500	200	600	200	1000	2450
MEL		1800		2600	3800	5000	1250
Jet Fighter		2500			1000		1500
Jet Transport		450		7000	3500	4000	550
Helicopter		50					250

#### 2.4 Flight Session Preparation

To achieve the objectives of the evaluation session, several tasks were conducted prior to the session. An overriding consideration was the round-robin format for the session which required six sailplanes and seven pilots to be brought together for a one week period. Since the pilots were available for a limited time, it was most important that the sailplanes be properly prepared in advance of the session. A constraint upon the session date was that it must occur early in the year so that the borrowed sailplanes would not be away from the owners during contest activities.

The session date was scheduled for May 1 thru May 6, 1976, so that University students could assist in the flight operations. With the grant awarded February 16, 1976, this session date would allow time for sailplane acquisition, pilot selection, sailplane checkout, instrumentation development and flight session planning. The schedule was tight but all objectives were accomplished.

The acquisition of the sailplanes was found to be much easier than anticipated. A few phone calls to members of the soaring community quickly revealed that the sailplanes of interest were available in the southeastern region of the U.S. The owners were most interested in assisting in this investigation.

Prior to the flight session, all sailplanes except 4 and 5 were acquired with sufficient time for a thorough inspection, airspeed calibration check, and weight and balance check. Sailplanes 4 and 5 were delivered by evaluation pilots and had prior checkout.

Sailplane 6 was acquired early and was used as a testbed for formulating the evaluation tasks and for the development of a simple sailplane data acquisition system. A battery powered signal conditioning unit was developed to give a digital display of either stick position or stick force to the pilot. It was found that small low friction potentiometers could be quickly attached to the sailplane control linkages, but the press of other flight activities and difficulties with pilot data recording limited the utility of quantitative data recording during the flight session. The stick forces were too low for the stick force balance borrowed from Dryden Flight Research Center and also the balance was too bulky for high performance sailplane control sticks.

## 2.5 Flight Session

The flight session was conducted May 1 through May 6, 1976. The weather was ideal throughout the session with a wide range of convection conditions present. The pilots were allowed to fly each of the ships as required to complete the evaluation questionnaires. Cassette recorders were used to record inflight comments to be used later during the evaluations. A maneuver list was supplied to further support the evaluation.

A total of ninety-eight flights were made for a total of 80 flying hours. The sailplane evaluation forms were completed during the session to maximize evaluation effectiveness. The pilots were most cooperative and willing to participate. The session was very flight intensive, yet all objectives were accomplished without any mechanical or safety problems.

## 2.6 Pilot Opinion Sampling Instruments and Data Presentation

The primary objectives of this study were to (1) obtain pilot opinion of the handling qualities of current high performance sailplanes, (2) to aid in the formulation of certification criteria, (3) to provide some guidance in future designs, and (4) to delineate areas which require further study. The most cost effective method to accomplish this task was to stage a round-robin

flight session in which seven test pilots evaluated six sailplanes representing distinct groups. The detailed sailplane handling quality pilot opinion data was obtained with a questionnaire which used the Cooper-Harper Rating Scale and pilot comments.

Questionnaire I (Appendix A) was designed to record the pilot's rating and comments of the sailplanes' handling qualities, design and cockpit layout. Each test pilot completed a questionnaire for each sailplane that he flew. The questionnaire was configured to evaluate the pilots' opinion of the sailplane handling qualities over the entire operating envelope from takeoff to landing. Specifically, each flight consisted of a tow to an altitude of 2700 or 3300 meters (AGL) depending on the pilot's preference. Evaluation tasks in smooth air were carried out before the flight reached lower altitudes (1000-1200 meters AGL) where convective conditions were usually encountered. On the average, the duration of each flight was 45 minutes, although some thermalling flight evaluations lasted as long as two hours. Evaluations were made in both smooth air and in thermalling flight to determine if there were any significant pilot opinion differences between the smooth air test conditions and the usual operational environment, that is under convective conditions. A set of maneuvers listed in Table 3 was flown by each pilot to provide a basis for the evaluations. The pilots made comments on cassette recorders during each flight and these comments were transcribed by the pilots to the questionnaires. The questionnaire included evaluations of the design and cockpit layout.

The Cooper-Harper Rating Scale (Reference 2), widely used in the evaluation of handling qualities of powered aircraft, was adopted for this questionnaire. The attractive feature of the Cooper-Harper Rating Scale, Figure 8, is the decision tree structure which guides the pilot to a number for his rating value. For this initial study, the interpretation of the rating scale was broadened to be used in the evaluation of such sailplane characteristics as ease of assembly, inspection, and cockpit layout. The key to this interpretation was the assumption that the pilots would compensate for deficiencies in the design as they would for deficiencies in flight stability and control. It should also be noted that only two of the seven pilots had extensive previous experience with the Cooper-Harper rating scale.



Table 3  
Evaluation Flight Tasks

A. Smooth Air Maneuver List

1. Evaluate take-off roll.
2. Evaluate tow characteristics; box tow plane.
3. Release, slow flight, stall entry, general characteristics.
4. Attain and maintain constant IAS: 50-70-90 kts. Evaluate trim capability over speed range. Note friction, noise, and vibration level.
5. Evaluate return to trim at 60 and 90 kts IAS.
6. Evaluate stick free stability. Trim at 60 and 90 kts. Introduce 5 kts airspeed perturbation and release stick. Note rate of convergence or divergence, time period of oscillation.
7. Evaluate stick position and force gradients over speed range. Trim at 75 kts, decelerate slowly to near stall then accelerate to 100 kts.
8. Evaluate pitch altitude response to small stick pulses over speed range especially at high speed (may be combined with Item 7).
9. Evaluate stick forces during pull up from high speeds.
10. Time roll rate during turn reversal (from 45° to 45° bank) at min. sink speed and at 65 kts. Evaluate ease of maintaining constant airspeed and coordination (zero sideslip).
11. Evaluate steady sideslip. Note force levels during rudder overbalance.
12. Evaluate constant g turn, 45° bank, 60 kts, L and R.
13. Evaluate constant g turn, 60° bank, 70 kts, L and R.
14. Evaluate flight path control system, pattern, flare characteristics, ease of touchdown control, landing roll.

B. Convective Flight Maneuver List

1. Evaluate takeoff, possibly crosswind effects, and tow characteristics in turbulence.
2. Evaluate stall/spin (incipient spin only) characteristics. Note onset of pre-stall buffet.
3. Thermalling characteristics
  - a. Low speed turns
  - b. Stall-spin susceptibility, recovery
  - c. Control characteristics near other aircraft
4. Interthermal flight evaluation. Fly at max L/D speed plus 10 kts and at rough air airspeed or 100 kts IAS (whichever is lower).
5. Evaluate handling during secondary task.
6. Evaluate glide path control, touchdown and rollout characteristics in turbulence.

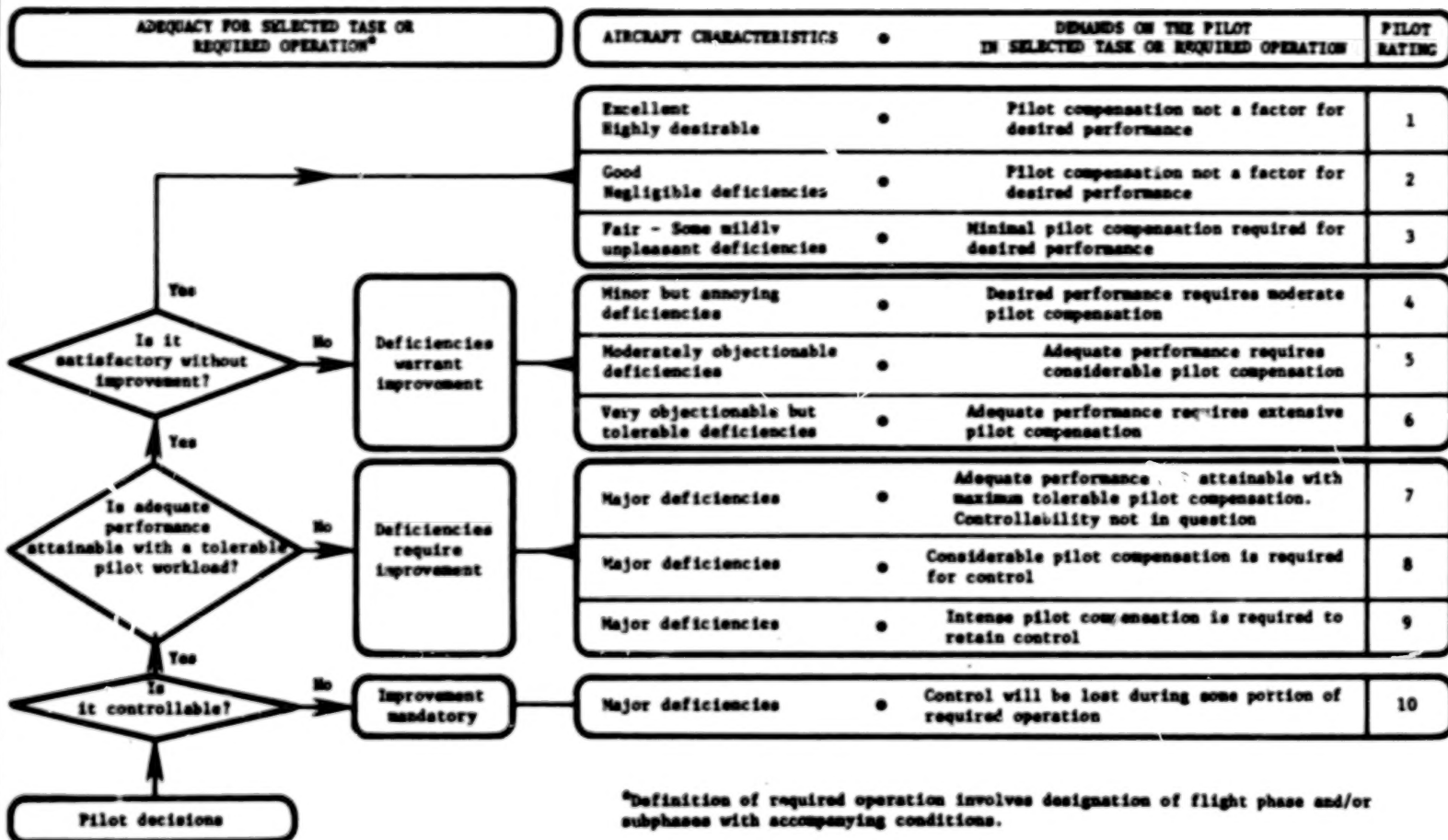


Figure 8. Cooper-Harper Rating Scale

Consequently, the other pilots had a tendency to use the Cooper-Harper Scale as a linear interval scale.

After the flight session was completed, the Cooper-Harper ratings and pilots' comments for each task of Questionnaire I were transcribed into a data file on the university mainframe computer to facilitate the analysis and presentation of the data. The Cooper-Harper Rating Scale, is not a linear scale, thus statistical techniques do not strictly apply. However, averages and standard deviations were computed to gain some measure of the consensus of pilot opinions. An average and standard deviation of all sub tasks for each pilot were computed to allow correlation of the average of sub tasks ratings with the major task rating. The pilots' responses to Questionnaire I are given in Appendix B. The format adopted was to group the responses of all pilots for all sailplanes covering a major area of interest such as longitudinal handling, etc. Extreme caution should be exercised in drawing conclusions from the numerically averaged ratings. As can be seen from the individual pilot ratings, different pilots used different standards of acceptance.

### 3. RESULTS AND DISCUSSION

#### 3.1 Pilot Rating Summaries

The Cooper-Harper Rating Scale is a valuable tool in the evaluation of aircraft handling qualities. To provide a measure of the variability of the pilot's assignment of ratings, averages and standard deviations for each task were computed for each sailplane. Again, it must be emphasized that the Cooper-Harper Rating Scale is non-linear and thus statistical methods do not strictly apply. Table 4 presents a summary of the average and standard deviation of all pilot ratings of a task for each sailplane. These average readings should not be directly compared with the levels of acceptability shown on the Cooper-Harper scale, but are rather a gross indication. Average Cooper-Harper ratings greater than 3.5 (with no specific meaning attached) have been underlined to delineate areas where problems were noted by most of the pilots. The standard deviations are a measure of the variation in the pilot's rating of a particular task.

Pilot rating numbers without their accompanying pilot comments are of very little value. The individual pilot ratings and comments furnished in Appendix A are rather formidable in their volume and scope. The numerical summaries of Table 4, rather than being accepted by the reader at their Cooper-Harper rating scale face value, should be used as a guide to point out sections of particular interest in the appendix pilot rating information.

Sailplanes 4 and 6 received poor ratings in construction and rigging. Sailplanes 4 and 5 rated down in cockpit layout, sailplanes 3 and 5 in longitudinal handling qualities, and sailplane 6 in stall/spin characteristics. Sailplanes 3, 4, and 5 were given poor ratings in landing characteristics, and sailplane 6 in circling flight. Sailplane 1 received consistently higher ratings than all other aircraft, in every rating category, and was often cited as a benchmark of excellence for sailplane handling qualities. To gain more than this superficial information, the reader must refer to the individual pilot comments in the above areas, which provide an understanding of the reasons for the ratings.

Table 4. Rating Summary for Sailplanes

TASK		SAILPLANE											
		1		2		3		4		5		6	
		Avg	STDV	Avg	STDV	Avg	STDV	Avg	STDV	Avg	STDV	Avg	STDV
1	I. Design	2.50	.50	2.00	.71	2.00	.71	<u>5.00</u>	1.00	2.00	.00	<u>4.50</u>	2.50
2	A. Pilot Opin. of Const. Rigging	2.00	1.00	1.37	.41	2.25	.43	<u>6.50</u>	.50	1.88	.22	<u>5.50</u>	1.50
3	1. Ease of Inspection	3.00	.82	1.50	.50	2.75	1.30	2.50	.50	1.75	.45	3.00	.00
4	2. Safety of Control System	2.00	.00	2.50	1.12	1.75	.43	3.50	1.50	1.75	.43	2.00	.00
5	3. Ease of Assembly	2.33	.47	1.25	.43	1.75	.43	<u>5.00</u>	1.00	2.00	.00	<u>6.00</u>	1.00
6	B. Pilot Opinion of Cockpit Layout	<u>3.60</u>	.49	2.60	.80	1.80	.75	<u>4.25</u>	1.48	1.70	.60	2.00	1.00
7	1. Pilot Comfort	3.29	.88	2.14	.99	1.14	.35	2.33	.75	1.40	.49	1.67	.75
8	2. Control System Arrangement	3.29	1.39	2.71	.70	3.00	1.41	<u>4.80</u>	1.60	2.75	1.48	2.67	.94
9	3. Instrument Display	2.57	.49	2.33	1.11	1.50	.50	2.00	.63	1.60	.49	2.80	.75
10	4. Pilot Visibility	3.29	.88	1.43	.73	1.86	.83	1.83	1.07	2.00	.89	1.67	.47
11	5. Pilot Safety	<u>2.75</u>	.83	<u>2.50</u>	.50	<u>2.50</u>	1.12	1.60	.49	<u>2.75</u>	1.30	1.00	.00
12	II. Smooth Air Maneuvering	1.12	.22	2.40	.49	2.33	.47	2.70	.00	3.00	1.26	1.25	.43
13	A. Pilot Opin. of Initial Takeoff Roll	1.67	.94	2.75	.99	2.57	.73	2.67	1.60	3.20	1.17	1.80	.75
14	1. Towline Backup	1.60	.49	2.17	.69	2.33	.94	1.17	.37	2.40	1.02	2.00	1.00
15	2. Control of Plane in Init. Roll	1.79	1.19	3.14	.99	2.57	.73	2.00	.58	3.20	1.17	1.83	1.07
16	B. Pilot Opinion of Tow	1.37	.41	2.20	.75	2.50	.50	2.20	.40	<u>3.50</u>	1.26	1.50	.50
17	1. Ease of Maintaining Position	1.43	.73	2.29	.70	2.29	.70	2.00	.00	2.80	1.33	1.67	.75
18	2. Aircraft Trim	<u>2.50</u>	1.34	2.57	.73	2.43	.49	2.50	1.26	2.20	.40	2.40	1.02
19	3. Control in Propwash	1.43	.73	2.14	.64	1.86	.64	2.17	.37	2.50	1.12	2.00	1.00
20	4. Release Characteristics	1.50	.50	1.67	.47	2.17	.69	1.80	.75	1.75	.43	1.83	.69

Table 4 (Continued)

TASK		SAILPLANE											
		1	2	3	4	5	6	7	8	9	10	11	12
		AVG	STDV	AVG	STDV	AVG	STDV	AVG	STDV	AVG	STDV	AVG	STDV
21	C. Pilot Opinion of Long-Handling	1.25	.43	2.60	.49	<u>4.10</u>	1.11	3.20	.75	<u>4.20</u>	1.33	2.67	.94
22	1. Ease of Rot & Main Con Airspeed	1.57	.90	2.43	.73	2.29	.45	2.67	.47	2.40	.80	2.00	.58
23	2. Plane Trim Sys. Over Speed Range	<u>2.86</u>	.64	3.00	.53	2.33	1.25	2.33	.94	2.60	1.20	2.60	1.02
24	3. Pitch Sensitivity	1.29	.45	2.79	.45	2.71	.70	2.17	.69	3.20	1.17	1.67	.47
25	4. Stick Force Gradient	1.57	.49	2.14	.99	2.29	1.03	3.17	1.07	2.80	1.17	2.33	1.25
26	5. Stick Fixed Stability	1.25	.43	1.50	.50	2.25	.43	2.00	.00	2.00	.00	2.00	.63
27	6. Stick Free Stability	1.17	.37	2.29	1.16	3.43	2.77	2.17	.69	<u>4.20</u>	2.93	2.20	.40
28	7. Return to Trim	1.83	.69	3.17	1.07	<u>3.80</u>	3.19	1.40	.49	<u>4.25</u>	3.42	1.80	.75
29	8. Manoeuvring Response	1.29	.45	2.86	.35	<u>2.71</u>	.88	2.17	.90	<u>5.60</u>	1.62	2.00	.58
30	9. Phugoid Characteristics	1.60	.49	2.83	.69	<u>5.29</u>	2.60	2.40	.49	<u>5.40</u>	2.58	2.00	.00
31	10. Dive Recovery	1.71	.45	2.71	.88	<u>4.00</u>	2.00	2.20	.98	<u>5.30</u>	1.78	2.00	.00
32	D. Pilot Opinion of Lateral Handling	1.00	.00	2.80	.75	2.20	.51	2.20	.40	2.60	.80	2.00	.00
33	1. Aileron Force Gradient	1.43	.49	2.14	.64	1.86	.64	2.17	.37	2.20	.40	2.00	.00
34	2. Rudder Force Gradient	1.43	.49	1.86	.83	2.29	1.03	2.17	.37	2.60	.49	2.17	.37
35	3. Roll Rate over Speed Range	2.00	.93	2.14	.35	1.86	.64	2.58	.45	3.30	1.08	2.50	.76
36	4. Sideslip Characteristics	2.00	.76	1.83	.69	2.86	.64	2.17	.50	2.80	.75	2.60	.49
37	5. Ease of Turn Entry	1.29	.45	2.71	.70	1.86	.64	2.00	.58	2.60	1.02	2.20	.75
38	6. Yaw Due to Aileron	2.00	.58	2.67	.75	2.17	.69	2.40	.80	3.00	1.55	2.50	.50
39	7. Yaw Due to Roll	2.00	.63	3.40	.49	2.20	.75	2.25	.63	2.00	.00	2.13	.94
40	8. Ease of Main. 45° Bank Turn	1.43	.73	1.86	.64	1.64	.69	2.00	1.00	1.20	.40	2.58	1.24
41	9. Ease of Main. 60° Bank Turn	1.57	.73	2.14	.64	1.93	.78	2.00	1.00	1.60	.49	2.83	1.07
42	E. Pilot Opin. of Plane Stallspin Char.	1.88	.74	2.20	1.60	2.40	1.02	3.00	.63	2.20	.75	<u>4.33</u>	1.25
43	1. Rudder, Aileron Effect Dur. Stall	2.09	.53	1.86	1.12	1.86	.64	2.33	.75	2.00	.63	<u>5.00</u>	1.15
44	2. Stall Warning	2.43	.49	2.71	1.39	2.43	.90	2.50	.76	2.20	.98	2.33	1.25
45	3. Aggravated Stall-Tend to Spin	2.00	1.00	2.14	1.73	2.57	.90	3.00	.58	2.20	.98	<u>4.00</u>	1.15
46	4. Stick Force Gradient	1.57	.73	2.00	.76	2.57	.73	2.00	1.00	2.60	.49	<u>2.33</u>	1.25
47	5. Stall Recovery, Altitude Loss	1.33	.47	1.67	.75	2.14	.64	1.80	.75	1.80	.75	<u>3.67</u>	1.89
48	6. Spin Entry	1.75	.83	3.00	1.41	2.33	.94	2.67	.47	2.00	.71	<u>4.50</u>	1.12
49	7. Spin Recovery	1.00	.00	1.50	.50	2.00	1.00	1.50	.50	2.50	.50	2.00	1.00
50	8. Stall From Turn at Low Speed	1.50	.50	1.86	1.12	2.67	.47	2.25	1.09	2.00	1.10	<u>4.00</u>	2.32

Table 4 (Continued)

SAILPLANE													
		1	2	3	4	5	6						
TASK		AVG	STDV	AVG	STDV	AVG	STDV	AVG	STDV	AVG	STDV	AVG	STDV
51	F. Pilot Opin. of Plane Landing Char.	1.70	.40	2.75	1.30	3.20	.40	<u>3.50</u>	.50	2.90	.66	2.33	.47
52	1. Pilot Visibility	2.57	.90	1.43	.73	1.43	.49	1.50	.50	1.40	.49	1.00	.00
53	2. Glide Slope Control	1.57	.73	3.00	.93	2.57	.49	2.67	.47	2.40	.49	1.33	.75
54	3. Airs. Control, Airb. Ease of Mod.	2.14	.99	3.14	.99	3.14	.35	<u>4.00</u>	.61	2.60	.49	1.60	.80
55	4. Ease of Land. at Intended Spot	1.57	.49	2.57	.73	2.57	.73	<u>5.87</u>	.40	2.40	.49	1.50	.50
56	5. Ease of Control, Sink at Touch	1.50	.50	2.29	.88	2.43	.9	<u>2.54</u>	.85	2.40	.49	1.80	.40
57	6. Control During Rollout	1.43	.73	2.57	.73	<u>4.00</u>	2.38	1.67	.47	<u>4.00</u>	1.26	1.33	.47
58	III. Flight Characteristics in Convexion	1.00	.00	2.50	.71	2.60	.49	2.62	.41	3.20	1.17	3.60	1.22
59	A. Pilot Opinion of Tow	1.50	.76	2.42	.84	2.42	.61	2.00	.00	<u>3.87</u>	1.43	2.25	.43
60	1. Ease of Maintaining Position	1.33	.75	2.50	.96	2.50	.50	2.00	.00	3.00	1.22	2.00	.00
61	2. Response to Vertical Currents	1.83	.69	2.50	.50	2.83	.69	2.00	.00	2.50	.50	2.00	.00
62	3. Balance	1.80	.40	1.75	.43	2.00	.63	2.33	.47	2.00	.82	2.00	.00
63	B. Pilot Opinion of Circling Flight	1.00	.00	2.40	.97	2.00	.00	2.87	.74	2.30	.75	<u>4.33</u>	2.62
64	1. Low Speed Handling	1.17	.37	2.83	.90	2.00	.58	2.75	.83	2.40	.49	<u>5.00</u>	2.16
65	2. Stall-Spin Susceptibility	1.75	.38	2.33	1.37	2.00	.58	2.37	.41	1.60	.49	<u>5.33</u>	2.87
66	3. Ease of Centering Thermal	1.83	.69	2.33	.75	2.00	.58	2.75	.43	2.75	1.09	<u>3.33</u>	.47
67	4. Speed Control	1.50	.50	2.17	1.21	2.33	.47	3.25	1.09	2.20	.98	<u>4.33</u>	1.25
68	C. Pilot Opinion of Cruising Flight	1.60	1.20	2.20	.98	2.60	.97	2.37	.65	2.20	.98	1.67	.47
69	1. Ease of Controlling Airspeed	1.67	1.11	2.17	.69	2.33	.94	2.37	.65	2.60	1.36	1.50	.50
70	2. Pull up 'eto Thermal	1.67	.47	2.00	1.15	2.00	.82	2.87	.89	2.00	.63	2.50	1.50
71	3. Ease of perf. Secondary Tasks	1.50	.50	2.50	1.12	2.00	.82	2.50	.50	3.20	1.94	1.50	.50
72	4. Ride Quality	2.17	.60	2.17	.37	2.73	.56	2.75	.43	1.80	.75	2.50	.50
73	5. Ease of Main. Strai, at Flight	1.40	.40	2.33	1.11	1.50	.50	1.75	.43	1.40	.80	1.75	.43



### 3.2 Pilot Evaluation of Ease of Assembly, Inspection and Cockpit Layout

Although these factors are generally not regarded as an essential part of handling qualities, as, say, longitudinal stability, all three characteristics do influence the ease and precision with which the pilot is able to perform tasks for the overall mission of the sailplane. In rating these characteristics, the pilots tended to disregard the dichotomous structure of the Cooper-Harper scale; instead, they were asked to rate these factors on a linear scale from one to ten. Also, three of the pilots did not rate the ease of assembly and inspection since the flight test session did not provide enough time for them to become familiar with these characteristics.

The pilots who rated the ease of assembly and ease of control system inspection generally gave better ratings to the newer machines. These pilot ratings also confirmed the fact that frequent assembly/disassembly is part of the high-performance sailplane role and the ease of assembly should be a very important design objective.

Pilot comments on the cockpit layout show that there were wide variations among the six evaluation sailplanes. The pilots found visibility was adequate in all ships. They singled out poor ventilation, the use of curved control sticks, confusing or unhandy secondary control handles (such as trim and flap handles), need for good pilot protection as areas of concern. The variety of adverse comments indicates the need of some sort of standardization for the location, shape and color of the secondary control handles.

### 3.3 Pilot Opinion of Longitudinal Characteristics

Takeoff. Average pilot ratings ranged from 1.8 for sailplanes 1 and 6 to 3.2 for sailplanes 2 and 5. Sailplanes 1 and 6 were generally the most stable, had the highest stick forces, and had strong damping of the short period pitching oscillation. Pilots commented that sailplane 2 was more sensitive in pitch than they liked, and that they tended to overcontrol in pitch during takeoff. On sailplane 5, pilots reported disliking the stick bobbing force and aft when rolling over bumps. One pilot felt it necessary to maintain greater ground clearance while he was airborne and waiting for the towplane to accelerate to takeoff speed than with other gliders and that wing flexing resulted in undesirable excursions in fuselage-to-ground



clearance. Although he gave a pilot rating of 2, one pilot noted that on sailplane 4, the longitudinal stick feel-and-trim spring system had high and unsymmetric breakout forces which caused him to overcontrol.

Tow. Again, pilot ratings were best for sailplanes 1 and 6, averaging 1.4 for 1 and 1.5 for 6. The worst average rating was 3.5 for sailplane 5. Pilots strongly objected to inertially induced stick forces, and reported overcontrolling, and a feeling that a serious PIO could occur. When the tow speed was increased from the standard 70 knots to 80 knots, the overcontrol/PIO tendency was reported more severe. One pilot reported he was unwilling to fly left-handed while raising the landing gear on tow. Sailplane 2 was reported easily upset in rough air, requiring frequent small control corrections. It received several pilot ratings of 3. Sailplane 4 was reported sensitive and easy to overcontrol, receiving pilot ratings of 2 and 3.

Establishing and Maintaining Airspeed. Establishing and holding speed was rated satisfactory for all sailplanes. It was reported by one pilot to be difficult to make fine speed corrections in sailplane 4 due to high breakout forces (his pilot rating was 2 however). For sailplane 5, one pilot reported that a pitch correction tended to continue past the intended point and had to be arrested by a checking control input, (his pilot rating was 4).

Longitudinal Trimming. The trim system on sailplane 1 was rated unsatisfactory. Comments were that it was ineffective and inconvenient. The trim system of every sailplane was reported as inconvenient to use, but only sailplane 1 was rated unsatisfactory. Comments indicated that pilots were content to fly without trimming rather than use inconvenient trim devices, except in the case of sailplane 6 in which stick forces became excessive.

Pitch Sensitivity. Sailplanes 3 and 5 received some pilot ratings of 4 and 5 for oversensitivity. Sailplanes 2, 3, 4, and 5 were described as sensitive, but 2 and 4 did not receive poor pilot ratings for sensitivity.

Stick Force Gradient, Stick Fixed Stability, and Stick Free Stability.

These were not tasks, but requests for opinions on the suitability of the listed characteristics. In the absence of quantitative data and since the pilot comments were rather general, the responses to these three requests for pilot opinion are broadly summarized: sailplane 1 was well liked; numbers 2, 3, and 5 were characterized as having light stick forces, bordering on too

light, while sailplanes 4, and, even more so, 6, were judged to have too-heavy stick forces.

Return to Trim. The pilots were satisfied with the return-to-trim characteristics of all sailplanes, giving pilot ratings of 2 to 3. An exception to this was pilot 1 who apparently excited the phugoid mode on this test and rated phugoid damping. Two pilots felt the task had no relevance to their opinion of a sailplane's handling qualities. Early NACA flying qualities tests by Gilruth (Reference 3) also showed that the tendency to return to trim speed was relatively unimportant for visual flight.

Maneuver Response. Opinions diverged on the maneuvering responses of the six sailplanes. Sailplane 1, 4, and 6 were well liked by all pilots, receiving mostly 1 and 2 pilot ratings. Sailplane 2 received mostly 3 ratings and comments giving the impression it was more responsive than the pilots liked. Sailplanes 3 and 5 got mixed opinions. Sailplane 3 was rated 4 and sailplane 5 rated 5 due to low or nil stick-force-per-g by some pilots. Delayed g response due to the flexible wing was reported to cause difficulty in stabilizing rapidly applied g by one pilot.

Phugoid Characteristics. This was not a flying task susceptible to pilot rating. Nonetheless pilots expressed their opinions of the suitability of the characteristic. Pilots were satisfied with the lightly damped or neutral stick-free phugoids of sailplanes 1, 2, 4, and 6, while some pilots objected to the strongly divergent stick-free phugoids of sailplanes 3 and 5. The divergent motions appeared to be caused by a dynamical interaction between the sailplane phugoid mode and the pitch control system.

Dive Recovery. Sailplanes 1, 4, and 6 were regarded as satisfactory. Sailplane 2 was given satisfactory pilot ratings, but several comments suggested that it was more sensitive than desired. Sailplanes 3 and 5 were rated unsatisfactory by some pilots who commented that the stick forces were too light, and sometimes reversed during pull-outs.

Ease of Centering Thermal, and Speed Control in Circling Flight. All sailplanes were rated satisfactory for these tasks. Comments indicated that the high stick forces and heavy stability of sailplane 6 caused an undesirably high workload in circling at varying bank angles as is typically done in thermalling flight. On sailplane 3, comments noted that the very low or negative stick-force-per-g was very pleasant to fly and felt immediately

natural and comfortable during the thermalling task. On sailplane 5 the same comments were made, and additionally that in an established thermalling turn the stick could be moved as much as 7 cm aft without appreciably affecting the turn. This later characteristic was not felt objectionable.

Table 5  
Sailplane Longitudinal Stability and Control Characteristics

<u>Sailplane</u>	<u>Control Forces</u>	<u>Trim</u>	<u>Static Longi- tudinal Stab.</u>	<u>Stick-Free Short Per. Damping</u>	<u>Stick Force Per G</u>	<u>Perceived Sensitivity</u>
1	Aerodynamic + Spring	Spring	Moderate	High	Mod- erate	Moderate
2	"	"	Lo	"	Lo	High
3	Spring + Bobweight	"	"	"	Nil	"
4	Aerodynamic + Spring	"	"	"	Lo	"
5	Spring + Bobweight	"	"	"	Nil	"
6	Aerodynamic	Tab	High	"	Mod- erate	Moderate

Table 6  
Summary of Opinions on Longitudinal Handling Qualities

<u>Sailplane</u>	<u>Takeoff and Tow</u>	<u>Straight Flight</u>	<u>Maneuvering &amp; Dive Pull-Out</u>	<u>Thermalling</u>
1	Well Liked	Well Liked	Well Liked	Well Liked
2	Satisfactory	Satisfactory	Satisfactory	Satisfactory
3	Satisfactory	Well Liked	Satisfactory	Well Liked
4	Satisfactory	Satisfactory	Satisfactory	Satisfactory
5	Satisfactory	Well Liked	Unsatisfactory	Well Liked
6	Well Liked	Well Liked	Well Liked	Satisfactory

Table 5 summarizes the longitudinal stability and control characteristics of the sailplanes evaluated and Table 6 summarizes the pilot opinion of longitudinal handling qualities for primary flight tasks. Table 6 shows that longitudinal characteristics best liked for thermalling are less well liked for takeoff, tow, maneuvering, and dive pull-out. From Table 5 it appears that increased stability and reduced sensitivity are beneficial to the first three tasks while lower stability and greater sensitivity are desirable for the last task. Table 6 shows that all the sailplanes had satisfactory or better longitudinal handling qualities for normal flying and thermalling, and that all but one were also satisfactory for maneuvering and dive pull-out. This was not surprising since all of the evaluation sailplanes were commercially successful in series production.

### 3.4 Sailplane Lateral-Directional Handling Qualities

Sailplane performance growth has not influenced lateral-directional handling qualities as much as the longitudinal handling qualities, although both have been degraded. The only serious lateral-directional problem apparent in current high performance sailplanes is in takeoff and landing, where low roll control and rudder power can lead to loss of directional control, especially in crosswinds. One cause is the placement of the landing wheel ahead of the C.G., which increases weather cock tendencies. Another is a raised C.G. coupled with a further aft and lower placement of the tow line attach point, which introduces a significant rolling moment with sailplane heading/tow line misalignment. This problem warrants further study to better define controllability during takeoff and landing.

Although pilot comments did not reflect any serious inflight problems, improvement in lateral-directional handling qualities, such as roll response quickening, increased roll control power, and reduction in rudder coordination requirements, would enhance performance in soaring flight, due to the importance of quickly acquiring and centering the thermals and of reducing pilot workload. Informal discussions with the evaluation pilots, as well as reported pilot comments, support this conclusion. Pilot opinions were mostly in the "excellent" to "minor but annoying deficiencies" region (pilot ratings 1 to 4).

Sailplane 1 was "excellent" to "good" (pilot rating 1 to 2) in almost every area. Pilot comments emphasized the good control harmony between rudder and aileron and ease of rudder-aileron coordination. Spiral stability was neutral, which was noted as beneficial for thermalling flight.

Sailplane 2 pilot ratings ranged from 2 to 4, with many comments about high rudder coordination workload in maintaining ball-in-the-center flight, both in turns and turn entries as well as level flight. Inadequate rudder control power was cited, as evidenced by insufficient rudder to maintain balanced flight in moderate rate turn entries. Spiral stability was slightly negative in thermalling configuration, which increased rudder-aileron coordination problems. Lateral-directional characteristics for this sailplane could be summarized as distracting and irritating. One pilot commented negatively on pitchup with sideslip, which is peculiar to this sailplane.

Pilot ratings for sailplanes 3, 4, and 5 fell in the 1 to 4 range. In average overall pilot ratings, sailplane 3 was slightly better than sailplanes 4 and 5, but ratings for each sailplane showed different areas of emphasis, as indicated in the following paragraphs.

Sailplane 3 lateral-directional control harmony and coordination was good. Comments ranged from "no problem" to "pleasant". Comments showed, however, that sailplane 1 was better. A comment for sailplane 3 on aileron effectiveness was that ailerons remained very effective even below stall speed.

The only complaints for sailplane 4 were due to the requirement for considerable top aileron in turning flight and mild objection to coordination workload in lateral maneuvering.

Sailplane 5 received good to excellent ratings for its ease of control in maintaining desired bank angles in turning flight. Several pilots objected to its low maximum roll rate of about 15 deg/sec, about 5 deg/sec less than that of all the other sailplanes, though 2 pilots commented that roll rate was surprisingly good for a sailplane of this large a wing span. Other comments indicated that the rudder force gradient was too high and noted too wide a deadband around neutral for airplane response to rudder inputs.

Sailplane 6 was judged as a training sailplane, suitable for transitioning into high performance ships. In this context, it received very good ratings, except for ease of maintaining desired bank angles and for control near the stall. Concerning turning flight, pilots commented that rudder forces were



too high relative to longitudinal stick forces and that unintentional overcontrolling in pitch produced frequent pre-stall airframe buffeting. Lateral control near stall was poor due to decaying roll control power with airspeed decrease.

Rudder overbalance, or "rudder lock" was a characteristic common to sailplanes 2, 3, and 5. The pilots did not find this unsafe or even annoying, except on sailplane 5; one pilot gave sideslips a rating of 4 due to this feature, noting that about 180 N pedal force was required to "unlock" the rudder and that large sideslip angles were possible. Control, however, remained good and very little buffeting occurred at the high sideslip angles. This is classified as a minor but annoying deficiency. Rudder overbalance on the other sailplanes required much less pedal force to unlock. It is concluded that although proportionally increasing rudder pedal force with rudder deflection is a desirable characteristic, rudder overbalance is not unsafe unless very high pedal forces or other overruling characteristics are involved. For instance, sailplane 2 encountered overbalance at about 1/2 rudder deflection and sailplanes 3 and 5 at about 3/4 deflection. These conditions were acceptable, but it might be that overbalance of significantly less rudder deflection would be unacceptable.

### 3.5 Sailplane Stall/Spin Characteristics

Cross-country soaring flight sometimes involves steep turns at low altitudes to take advantage of whatever lift may be available, avoiding landing unless absolutely necessary. Since optimum airspeed for thermalling flight is near the stall speed, stall and incipient spin characteristics are of prime importance in safety of flight.

Stall warning characteristics of the evaluation sailplanes were described as mild for sailplanes 1 through 5 and too much for sailplane 6. The airspeed stall warning band varied from 1 to 3 kts for the first 4 sailplanes, and were often in a form that could be masked by atmospheric turbulence. However, once the stall was recognized, recovery in most cases was easily and quickly effected by merely relaxing aft stick pressure and flying out of the stalled condition with little altitude loss. Sailplane 6, on the other hand, had a wide stall warning airspeed band of 10-12 kts, which caused stall buffet to

occur frequently at thermalling flight airspeeds. The pilots noted that this is an undesirable characteristic because familiarity with the stall warning buffet degrades its effectiveness and tends to cause the pilot to ignore the warning.

As to stall, incipient spin, and recovery characteristics, sailplanes 1, 2, 3, and 5 generally received good to excellent ratings with sailplane 1 being foremost. Good aileron control was noted, even below stall speed, and abused, cross-controlled stalls did not reveal undesirable qualities. Sailplane 4 recovered immediately with relaxation of aft stick force, but two pilots noted a definite autorotative (spin) tendency if recovery was not executed promptly with wing drop. Sailplane 6 showed a tendency to yaw and roll to the left and to pitch down from a cross-control stall and received lower ratings due to this characteristic toward spinning.

### 3.6 Sailplane Approach and Landing Characteristics

Once committed to landing, sailplanes cannot go up; it follows that one of the primary considerations in evaluating approach and landing characteristics is ease of glidepath control. Precision in touchdown control is paramount for landing in unprepared and restricted areas, a situation often encountered in cross-country soaring flight. It is therefore not surprising that most of the evaluation sailplanes were criticized for lack of spoiler, flap, or air-brake effectiveness and precision.

Sailplane 6 received the best ratings, in the fair to good category, largely because of the effectiveness of spoilers in controlling glidepath. For instance, one pilot noted that due to dive brake effectiveness, it was easy to make "difficult" landings. "Difficult" here means landings over obstructions into a limited landing area.

Sailplane 1 again received the best rating of all except sailplane 6, although it was noted that the divebrakes were somewhat ineffective. The same comment was made about sailplanes 2, 3, and 5. Sailplane 4 relied only on flaps for glidepath control. This concept was criticized on two points: large changes in pitch attitude with varying degrees of flap extension made precise glidepath control more difficult, and awkward placement, high force requirements, and complex flap control positioning requirements degraded precision of

glidepath control. Some pilots criticized the "suck-open" tendency of spoiler controls on the other sailplanes for the same reasons; the necessity to hold force to restrain spoiler control lever aft movement degraded precise control in pitch with light stick forces, especially if spoiler control forces were high.

It is concluded that more quantitative information should be gathered on primary glide path control capability and also interaction of glide path controls with primary flight controls.

### 3.7 Pilot Opinion and Certification Criteria

Pilot opinion specifies the characteristics pilots like in sailplanes. Certification criteria specify the characteristics thought by the certifying authority to be essential to their safe operation. There is no reason to expect that pilots will invariably prefer a safer characteristic to one less safe. The contribution to safety of a given characteristic sometimes being recognizable only by a complex analysis or demonstrated in accident patterns. However, in the absence of such analysis or evidence, it would seem sensible that criteria should conform in general to favorable pilot opinion.

General and specific examples of conflicting criteria and pilot opinion follow:

In general, pilots were willing to accept sailplanes that were somewhat more sensitive and less stable in pitch than they liked for take-off, tow, and dive recovery in order to get easy longitudinal maneuvering and low stick forces for soaring flight--the mission of a sailplane. In particular, the criteria specifying a return-to-trim within, say, 10 percent of trim speed was felt to be of no benefit, and when achieved through increased stick centering forces considered to be a harassment. In what way such a criterion is essential to safety is not clear.

The only undesirable characteristic exhibited by some of the high performance sailplanes was marginal control during takeoff and landing. Current certification requirements are vague in this area. A requirement of controllability during takeoff and landing in crosswinds up to a prescribed level would be appropriate.



The requirement that no rudder overbalance occur was considered by some pilots to be overly restrictive. They argued that the natural instinct to straighten out would be sufficient to cue the pilot to overcome the mild overbalance that commonly occurs on gliders at large sideslip angles.

The sailplanes flown illustrated the ways in which stalling behavior desirable for sailplanes differs from that desirable for power planes. First, pre-stall warning was found to be of little or no value because of the normal course of thermalling, the stall boundary is commonly exceeded--an alarm quickly loses its value when often sounded. In any case, regardless of the presence or absence of any pre-stall warning, the considerable loss of climb that would result from reacting to every momentary gust-induced stall warning is unacceptable to most sailplane pilots. They will maneuver as the thermal demands and accept brief occasional stalls. Because occasional stalls must be accepted, it is important that only the least reduction in angle-of-attack be sufficient to achieve an immediate unstall, and that very little loss in altitude and very minor upset accompany the stall. Fortunately, this was just the behavior observed for all the sailplanes except sailplane 6 which had considerable altitude loss and some roll and yaw upset. For deeper or more prolonged or abused stalls, traditional criteria appeared acceptable. Thus, a modification to the traditional criteria such that the initial stall replaced buffet as a warning, and the deeper or aggravated stall be treated as the stall for purposes of certification.

The drag modulation observed on the test sailplanes was felt to be generally insufficient and the operating forces for the drag devices were felt to be generally undesirable for both flaps and airbrakes. Additionally, the variation of divebrake or flap effectiveness during the flare, float and touch-down phase was felt to degrade the pilots' ability to control his landing accuracy. In view of the importance of accurate landings for sailplanes, it was felt that a rational basis should be established for future criteria.

#### 4. CONCLUDING REMARKS

The handling qualities of six sailplanes were evaluated by seven pilots in a flight test session consisting of 98 flights. The term "handling qualities" was defined to be those broad characteristics or attributes which influence the ease and precision with which the pilot is able to perform tasks for the overall mission of the sailplane. In this context the evaluation pilots were instructed to regard cross-country flight under visual flight rules as the principal mission of the sailplane.

Sailplane characteristics were evaluated using the Cooper-Harper rating scale with additional comments. The pilot opinion data indicates the following:

1. The evaluation sailplanes were found generally deficient in the area of cockpit layout. Poor cockpit ventilation, the use of curved control stick, confusing secondary control handles and the need for better cockpit crashworthiness were cited as reasons for deficiency.
2. The pilots indicated general dissatisfaction with pitch sensitivity which in some cases was coupled with inertially induced stick forces. While all sailplanes were judged satisfactory for centering thermals and in the ease of speed control in circling flight, pilot opinions diverged on the maneuvering response, pull-out characteristics from a dive, and on phugoid damping. The pilots found that the tendency to return to trim airspeed is relatively unimportant for visual flight.
3. Lateral-directional control problems were noted mainly during takeoff and landing. Pilot comments indicate the desirability of overall improvements in roll response quickening, increasing roll control power and reduction in the rudder coordination requirement. Existing levels of rudder overbalance or "rudder lock" was not found unsafe or even annoying.
4. Five of the evaluation sailplanes had very narrow airspeed band in which perceptible stall warning buffet occurred. This was not objectionable, however, since stall recovery was easy. The pilots objected to the characteristics of wide airspeed band of stall warning followed

by a stall with yawing and rolling tendency and substantial loss of altitude during the stall.

5. Landing characteristics of the evaluation sailplanes were found generally objectionable. Ineffective divebrakes, and the necessity of exerting a force to restrain divebrake control lever were quoted by some of the pilots. Flap type glide path control was also rated deficient due to the large attitude changes accompanying flap deflections and to the excessive flap actuation forces.

The present study shows the need for a more quantitative investigation of the factors influencing pitch control sensitivity such as precise measurements of stick forces due to both the aerodynamic hinge moments and the bobweight effects arising from the different horizontal tail configurations. Further study is required of lateral-directional control during takeoff and landing. More quantitative information should be gathered also on the various glide path control systems and the interaction of glide path controls with primary flight controls.

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Appendix A  
Pilots' Questionnaire

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Appendix A.  
Questionnaire

SAILPLANE EVALUATION

Pilot \_\_\_\_\_ Sailplane \_\_\_\_\_  
Date \_\_\_\_\_ Flight No. \_\_\_\_\_

I. Design. . . . . ☐

A. Pilot Opinion of Construction & Rigging. . . . . ☐

1. Ease of Inspection. . . . . ☐

2. Safety of Control System. . . . . ☐

3. Ease of Assembly. . . . . ☐

4. Comments \_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_

B. Pilot Opinion of Cockpit Layout. . . . . ☐

1. Pilot Comfort. . . . . ☐

2. Control System Arrangement. . . . . ☐

3. Instrument Display. . . . . ☐

4. Pilot Visibility. . . . . ☐

5. Pilot Safety. . . . . ☐

6. Comments \_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_

II. Smooth Air Maneuvering. . . . .

☐

A. Pilot Opinion of Initial Takeoff Roll. . . . .

☐

1. Towline Hookup. . . . .

☐

2. Control of Sailplane During Initial Roll. . . . .

☐

3. Comments \_\_\_\_\_

B. Pilot Opinion of Tow. . . . .

☐

1. Ease of Maintaining Position. . . . .

☐

2. Aircraft Trim. . . . .

☐

3. Control in Propwash. . . . .

☐

4. Release Characteristics. . . . .

☐

5. Comments \_\_\_\_\_

C. Pilot Opinion of Longitudinal Handling. . . . .

☐

1. Ease of Establishing and Maintaining a  
Constant Airspeed. . . . .

☐

2. Sailplane Trim System Over Speed Range. . . . .

☐

3. Pitch Sensitivity. . . . .

☐

4. Stick Force Gradient. . . . .

☐

5. Stick Fixed Stability. . . . .

☐

6. Stick Free Stability. . . . . ☐
7. Return to Trim. . . . . ☐
8. Maneuvering Response. . . . . ☐
9. Phugoid Characteristics. . . . . ☐
10. Dive Recovery. . . . . ☐
11. Comments \_\_\_\_\_
- \_\_\_\_\_
- \_\_\_\_\_

D. Pilot Opinion of Lateral Handling. . . . . ☐

1. Aileron Force Gradient. . . . . ☐
2. Rudder Force Gradient. . . . . ☐
3. Roll Rate Over Speed Range. . . . . ☐
4. Sideslip Characteristics. . . . . ☐
5. Ease of Turn Entry. . . . . ☐
6. Yaw Due to Aileron. . . . . ☐
7. Yaw Due to Roll. . . . . ☐
8. Ease of Maintaining 45° Bank Turn. . . . . ☐
9. Ease of Maintaining 60° Bank Turn. . . . . ☐

10. Comments \_\_\_\_\_
- \_\_\_\_\_
- \_\_\_\_\_

E. Pilot Opinion of Sailplane Stall-Spin Characteristics ☐

1. Rudder and Aileron Effectiveness During Stall ☐
2. Stall Warning. . . . . ☐
3. Aggravated Stall-Tendency to Spin. . . . . ☐
4. Stick Force Gradient. . . . . ☐
5. Stall Recovery, Altitude Loss. . . . . ☐
6. Spin Entry. . . . . ☐
7. Spin Recovery. . . . . ☐
8. Stall From Turn at Low Speed. . . . . ☐

9. Comments \_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_

F. Pilot Opinion of Sailplane Landing Characteristics. ☐

1. Pilot Visibility. . . . . ☐
2. Glide Slope Control. . . . . ☐
3. Airspeed Control, Airbrake Ease of Modulation ☐
4. Ease of Landing at Intended Spot. . . . . ☐
5. Ease of Controlling Sink at Touchdown. . . . ☐
6. Control During Rollout. . . . . ☐

7. Comments \_\_\_\_\_  
\_\_\_\_\_

---

III. Flight Characteristics in Convection. . . . . ☐

A. Pilot Opinion of Tow. . . . . ☐

1. Ease of Maintaining Position. . . . . ☐

2. Response to Vertical Currents. . . . . ☐

3. Release. . . . . ☐

4. Comments \_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_

B. Pilot Opinion of Circling Flight. . . . . ☐

1. Low Speed Handling. . . . . ☐

2. Stall-Spin Susceptibility. . . . . ☐

3. Ease of Centering Thermal. . . . . ☐

4. Speed Control. . . . . ☐

5. Comments \_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_

C. Pilot Opinion of Cruising Flight. . . . . ☐

1. Ease of Controlling Airspeed. . . . . ☐

2. Pull up into Thermal. . . . . ☐

3. Ease of Performing Secondary Tasks. . . . . ☐

4. Ride Quality. . . . . ☐

5. Ease of Maintaining Straight Flight. . . . . ☐

6. Comments \_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_

**Appendix B**  
**Cooper Harper Ratings and Pilots' Comments**

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\*\*\*\*\* ZEROS INDICATE NO RATING BY PILOT \*\*\*\*\*

# SAILPLANE 1 DATA

TASK	DESCRIPTION OF TASKS	1	2	3	PILOT	5	6	7	AVER.	STD DEV					
UNCLASS	1. DESIGN	.00	.00	3.00	.00	.00	2.00	.00	2.400	.500					
	A. PILOT OPIN. OF CONST. & RIGGING	.00	.00	3.00	.00	.00	1.00	.00	2.000	1.000					
	1. EASE OF INSPECTION	.00	.00	3.00	.00	.00	2.00	.00	3.000	.816					
	2. SAFETY OF CONTROL SYSTEM	.00	.00	3.00	.00	.00	3.00	.00	2.000	.000					
	3. EASE OF ASSEMBLY	.00	.00	3.00	.00	.00	2.00	.00	2.333	.471					
74	AVER. AND STD. DEV. OF SUBTASKS(EX 1:2:..)	.0	.0	2.7	.0	2.7	.5	.0	.0	2.0	.0	.0	.0	2.4	.68

TASK	PILOT	COMMENTS
2	3	NOT AS GOOD AS GLASS SHIPS
2	3	HAVE TO REMOVE OVERWING FAIRING
2	3	GOOD
2	3	MODERATELY EASY
74	0	AFTER ASSEMBLY, INSPECTION IS DIFFICULT AT ELEVATOR AND WING PINS
74	0	AILERON CONNECTION

# SAILPLANE 2 DATA

TASK	DESCRIPTION OF TASKS	1	2	3	PILOT	5	6	7	AVER.	STD DEV						
1	1. DESIGN	2.00	1.00	3.00	.00	.00	2.00	.00	2.000	.707						
1	A. PILOT OPIN. OF CONST. & RIGGING	1.50	.00	.00	.00	.00	2.00	.00	1.375	.415						
1	1. EASE OF INSPECTION	.00	.00	.00	.00	.00	2.00	.00	2.000	.500						
1	2. SAFETY OF CONTROL SYSTEM	1.00	.00	.00	.00	.00	2.00	.00	2.400	1.118						
1	3. EASE OF ASSEMBLY	1.00	1.00	1.00	.00	.00	2.00	.00	1.950	.433						
74	AVER. AND STD. DEV. OF SUBTASKS(EX 1:2:..)	1.3	.5	1.3	.5	1.7	.0	.0	.0	.0	2.7	.0	.0	.0	1.7	.92

TASK	PILOT	COMMENTS
74	3	EXCELLENT
74	3	APPEARS MECHANICALLY OF MARGINAL DURABILITY
74	3	POSSIBLE TO GET AILERON MOVEMENT WITH DISCONNECTED PUSH RODS
74	3	OUTSTANDING
74	3	HAS POOR HISTORY FOR RUDDER ACTIVATION SYSTEM. ELEVATOR, AILERON
74	3	AND FLAP SYSTEM IS EXCELLENT
74	3	AILERONS CONTROL RODS ENDS, CAN BE INSTALLED BUT NOT PINNED.
74	3	OTHERWISE IT IS BY FAR THE BEST ASSEMBLY OF ANY SAILPLANE.

# SAILPLANE 3 DATA

TASK	DESCRIPTION OF TASKS	1	2	3	PILOT	5	6	7	AVER.	STD DEV
1. DESIGN	1. PILOT OPIN. OF CONST. & RIGGING	2.00	1.00	2.00	.00	.00	3.00	.00	2.000	.707
	1. EASE OF INSPECTION	2.00	.00	.00	.00	.00	3.00	.00	2.000	.433
	2. SAFETY OF CONTROL SYSTEM	2.00	.00	.00	.00	.00	3.00	.00	2.000	1.000
	3. EASE OF ASSEMBLY	2.00	.00	1.00	.00	.00	2.00	.00	1.750	.433
	74 AVER. AND STD. DEV. OF SUBTASKS(EX 1:2:..)	1.7	.5	2.0	.0	1.7	.5	.0	.0	3.0

TASK	PILOT	COMMENTS
74	3	EXCELLENT
74	3	NOT AS EASY AS SAILPLANE 2 OR 5
74	3	UNABLE TO VISUALLY INSPECT AILERON CONNECTORS BEHIND SPAR
74	3	GOOD
74	3	EXCELLENT
74	3	QUALITY OF CONSTRUCTION IS EXCELLENT--AILERON AND AIR BRAKE LINKAGES

\*\*\*\*\* ZEROS INDICATE NO RATING BY PILOT \*\*\*\*\*

#### SAILPLANE 4 DATA

TASK	DESCRIPTION OF TASKS	1	2	3	PILOT 4	5	6	7	AVER.	STD DEV
1	1. DESIGN	.00	.00	2.00	.70	.00	6.00	.00	5.000	1.000
2	A. PILOT OPIN. OF CONST. & RIGGING	.00	.00	2.00	.70	.00	6.00	.00	5.000	1.000
3	1. EASE OF INSPECTION	.00	.00	2.00	.70	.00	6.00	.00	5.000	1.000
4	2. SAFETY OF CONTROL SYSTEM	.00	.00	2.00	.70	.00	6.00	.00	5.000	1.000
5	3. EASE OF ASSEMBLY	.00	.00	2.00	.70	.00	6.00	.00	5.000	1.000
74	AVER. AND STD. DEV. OF SUBTASKS(EX 1:2+...)	.0	.0	.0	4.7	1.2	.0	.0	2.7	1.49

TASK	PILOT	COMMENTS
75	1	LESS DESIRABLE THAN MOST
76	2	GOOD
77	3	FIND BENDING OF HANDLE REQUIRED FOR FLAP ACTUATION OBJECTIONABLE
78	4	MORE DIFFICULT THAN OTHERS
79	5	CANOPY FITS FAIRLY BADLY BEFORE LOCKING. FO AND TRIM AND FLAP HANDLE
80	6	ACTUATION CHARACTERISTICS OBJECTIONABLE.
81	7	ASSEMBLY NOT COMPARING WITH TASK. I.E. FREQUENT ASSEMBLY/DISASSEMBLY
82	8	IN MINIMUM TIME WITH 2-3 PEOPLE

#### SAILPLANE 5 DATA

TASK	DESCRIPTION OF TASKS	1	2	3	PILOT 4	5	6	7	AVER.	STD DEV
1	1. DESIGN	2.00	.00	2.00	.70	.00	2.00	.00	2.000	.000
2	A. PILOT OPIN. OF CONST. & RIGGING	2.00	.00	2.00	.70	.00	2.00	.00	2.000	.000
3	1. EASE OF INSPECTION	2.00	.00	2.00	.70	.00	2.00	.00	2.000	.000
4	2. SAFETY OF CONTROL SYSTEM	2.00	.00	2.00	.70	.00	2.00	.00	2.000	.000
5	3. EASE OF ASSEMBLY	2.00	.00	2.00	.70	.00	2.00	.00	2.000	.000
74	AVER. AND STD. DEV. OF SUBTASKS(EX 1:2+...)	1.7	.5	2.0	.0	1.7	.5	.0	.0	1.8

TASK	PILOT	COMMENTS
75	1	OUTSTANDING
76	2	EXCELLENT-EASIER THAN SOME SMALLER SHIPS
77	3	EXCELLENT CONSTRUCTION-FAIRLY LARGE FREEPLAY WAS OBSERVED IN THE
78	4	HORIZONTAL TAIL SURFACE ATTACHMENT
79	5	HEAVY BUT SIMPLE ONCE TECHNIQUE IS UNDERSTOOD

#### SAILPLANE 6 DATA

TASK	DESCRIPTION OF TASKS	1	2	3	PILOT 4	5	6	7	AVER.	STD DEV
1	1. DESIGN	.00	.00	2.00	.70	.00	7.00	.00	4.500	2.000
2	A. PILOT OPIN. OF CONST. & RIGGING	.00	.00	2.00	.70	.00	7.00	.00	4.500	2.000
3	1. EASE OF INSPECTION	.00	.00	2.00	.70	.00	7.00	.00	4.500	2.000
4	2. SAFETY OF CONTROL SYSTEM	.00	.00	2.00	.70	.00	7.00	.00	4.500	2.000
5	3. EASE OF ASSEMBLY	.00	.00	2.00	.70	.00	7.00	.00	4.500	2.000
74	AVER. AND STD. DEV. OF SUBTASKS(EX 1:2+...)	.0	.0	.0	3.3	1.2	.0	.0	4.0	2.2

TASK	PILOT	COMMENTS
75	1	EXCELLENT
76	2	GOOD SOLID DESIGN. RIGGING IS MORE DIFFICULT THAN MOST. GOOD
77	3	SAFE CONTROL SYSTEM
78	4	SHIP IS SIMPLY NOT DESIGNED FOR ASSEMBLY/DISASSEMBLY
79	5	NECESSARY FOR A SAILPLANE.

\*\*\*\*\* ZEROS INDICATE NO RATING BY PILOT \*\*\*\*\*

# SAILPLANE 1 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV
8	B. PILOT OPINION OF COCKPIT LAYOUT	3.00	3.00	3.00	3.00	3.00	3.00	3.00	3.00	.000
9	1. PILOT COMFORT	3.00	3.00	3.00	3.00	3.00	3.00	3.00	3.00	.000
10	2. CONTROL SYSTEM ARRANGEMENT	3.00	3.00	3.00	3.00	3.00	3.00	3.00	3.00	.000
11	3. INSTRUMENT DISPLAY	3.00	3.00	3.00	3.00	3.00	3.00	3.00	3.00	.000
12	4. PILOT VISIBILITY	3.00	3.00	3.00	3.00	3.00	3.00	3.00	3.00	.000
13	5. PILOT SAFETY	3.00	3.00	3.00	3.00	3.00	3.00	3.00	3.00	.000
75	AVER. AND STD. DEV. OF SUBTASKS(1:2:..)	3.0	3.2	3.0	3.0	3.5	3.8	4.0	3.2	1.01

TASK	PILOT	COMMENTS
8	7	FAIR VERY UNCOMFORTABLE SIT TOO LOW IN A/T RUDDER PEDALS UNSIRABLE CHANGING TYPE STICK HITS LEG WITH FULL AILERON THROW PI INSTRUMENTS GOOD, HOWEVER COMPASS LOCATED TOO FAR FORWARD AND ALMOST REQUIRES LIGHT TO SEE NUMBERS VISIBILITY DOWN MARGINAL SIDES OF COCKPIT TOO HIGH WHICH REDUCES DOWN VISIBILITY NOT GOOD AFT OR FORWARD DOWN LIGHT GOODEN STRUCTURE PILOT PROTECTION MINIMAL PILOT COMFORT IS POOR, VISIBILITY IS RESTRICTED SOMEWHAT, INSUFFI- CIENT LEG SPACE, TOP HINGED RUDDER PEDALS TAKES SOME GETTING USED NEEDS CUSHIONS-LEGS INTERFERE WITH FULL AILERON-HARD TO SEE COMPASS SEAT BACK NOT PROPERLY DESIGNED, HEAD THROUGH (FISHBOWL) SEVERE CONCERN ABOUT PILOT PROTECTION, TOP HINGED RUDDER PEDALS UNSATISFAC- TORY LATERAL, DOWNWARD AND REARWARD VISIBILITY STICK TOO FAR FORWARD LONG, TRIM CONTROL TOO FAR FORWARD STIRRUP RUDDER PEDALS UNDERSTIRABLE EXCESSIVE AIR LEAKAGE IN COCKPIT SEAL.

# SAILPLANE 2 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV
8	B. PILOT OPINION OF COCKPIT LAYOUT	2.00	2.00	3.00	3.00	3.00	3.00	3.00	3.00	.000
9	1. PILOT COMFORT	2.00	2.00	3.00	3.00	3.00	3.00	3.00	3.00	.000
10	2. CONTROL SYSTEM ARRANGEMENT	2.00	2.00	3.00	3.00	3.00	3.00	3.00	3.00	.000
11	3. INSTRUMENT DISPLAY	2.00	2.00	3.00	3.00	3.00	3.00	3.00	3.00	.000
12	4. PILOT VISIBILITY	2.00	2.00	3.00	3.00	3.00	3.00	3.00	3.00	.000
13	5. PILOT SAFETY	2.00	2.00	3.00	3.00	3.00	3.00	3.00	3.00	.000
75	AVER. AND STD. DEV. OF SUBTASKS(1:2:..)	1.6	2.2	1.1	2.8	1.0	1.8	1.0	3.2	1.07

TASK	PILOT	COMMENTS
7	7	NOT VERY COMFORTABLE ARM OUTSTRETCHED TRIM LEVER IN POOR LOCATION--STICK TOO FAR FWD. TRIMMER TOO FAR BACK, HARD TO REACH AND HARD TO OPERATE AVERAGE STICK TOO FAR FWD. FACTORY STICK IS OK, TEST SHIP HAD A NON-STANDARD TYPE. ELECTRIC VARIO INOPERATIVE SHORTAGE OF INSTRUMENT/RADIO SPACE. VERY GOOD INADEQUATE PILOT PROTECTION DUE TO MINIMAL STRUCTURE VERY LIGHT STRUCTURE NOT A STRONG FEATURE OF THIS GLIDER SEAT BELT INSTALLATION WAS SUCH THAT SEAT BELT ADJUSTMENT WAS VERY DIFFICULT AND PROBABLY IMPOSSIBLE IN FLIGHT. POOR PROTECTIVE STRUCTURE. SEAT BELTS HARD TO ADJUST SHORT NON-STANDARD STICK WAS FOUND UNPLEASANT. DIVE BRAKE CAN COME OUT OF DETENT EVEN AFTER ADJUSTMENT. CONTROL STICK (NOSE) TOO FAR FWD. TRIM LOCATION POOR, DIFFICULT TO REACH THE TRIM LEVER BECAUSE OF NARROW COCKPIT. ALSO TRIM WAS FROM DETENT TO DETENT. THE DETENT SPACING WAS SUCH THAT IT DID NOT ALLOW TRIM A/T ADJUSTMENTS. RUDDER ADJUSTMENT WAS EXCELLENT. GOOD RUDDER ADJUSTMENT FIBERGLASS STRUCTURE IN THE FORM OF KEEL OR STRINGERS (LONG) WOULD IMPROVE LEG/FOOT SAFETY OF NOSE IMPACT INCIDENTS/ACCIDENTS TRIM CONTROL PLACEMENT AWARD TO USE

\*\*\*\*\* ZEROS INDICATE NO RATING BY PILOT \*\*\*\*\*

# SAILPLANE 3 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV	
9	B. PILOT OPINION OF COCKPIT LAYOUT	2.00	1.00	2.00	2.00	2.00	2.00	2.00	1.800	.728	
10	1. PILOT COMFORT	2.00	1.00	1.00	2.00	2.00	2.00	2.00	1.743	.520	
11	2. CONTROL SYSTEM ARRANGEMENT	1.00	1.00	2.00	2.00	2.00	2.00	2.00	1.850	1.414	
12	3. INSTRUMENT DISPLAY	1.00	1.00	1.00	2.00	2.00	2.00	2.00	1.850	.500	
13	4. PILOT VISIBILITY	3.00	2.00	2.00	2.00	2.00	2.00	2.00	2.857	.833	
14	5. PILOT SAFETY	3.00	3.00	3.00	2.00	2.00	2.00	2.00	3.500	1.118	
75	AVER. AND STD. DEV. OF SUBTASKS(1:2...)	2.0	.9	1.7	.8	2.0	.6	1.8	1.7	2.0	1.29

TASK	PILOT	COMMENTS
7	1	VERY GOOD, BETTER THAN SAILPLANE 2. COULD USE MORE VENTILATION
8	1	CONTROL STICK, RELEASE LEVER TOO FAR FWD.
9	1	EXCELLENT
10	1	TOO RELEASE HARD TO REACH, MAKE A LITTLE AWKWARD TO REACH.
11	1	ELEVATOR OFFSET SO THAT POSITIVE COL GIVES UP ELEVATOR INPUT, VERY
12	1	BAU AT SPEED.
13	1	VISIBILITY FWD COULD BE IMPROVED
14	1	NOT EVALUATED
15	1	FWD AND DOWN SLIGHTLY OBSCURED
16	1	VERY GOOD
17	1	COCKPIT CONSTRUCTION MINIMAL IN STRENGTH
18	1	GLASS FUSPLANE POOR ENERGY ABSORBER
19	1	NOT AS GOOD AS SAILPLANE 4
20	1	SEAT BELT INSTALLATION WAS SUCH THAT SEAT BELT ADJUSTMENT WAS
21	1	DIFFICULT, PROBABLY IMPOSSIBLE IN FLIGHT.
22	1	WENT OFF HUNG AND OVER A DITCH, NOTHING BROKEN BUT FEELINGS
23	1	SEAT BELT A LITTLE LOOSE, SO BOUNCED HEAD ON CANOPY. SEAT BELT
24	1	ADJUSTMENT DIFFICULT.
25	1	ADDITIONAL NOSE STRENGTH SHOULD BE ADDED TO PROTECT PILOT'S FEET/LEGS
26	1	IN CASE OF BAD LANDING.
27	1	INSTRUMENT PANEL TOO FAR FWD. ACTUALLY WITH CUSHIONS, THE PANEL
28	1	IS NOT DIRECTLY VISIBLE.
29	1	WOULD BE ACCESSIBLE FOR PEOPLE WITH SHORT REACH.
30	1	TOO RELEASE TOO FAR FROM PILOT. BRAKE HANDLE ON CONTROL STICK
31	1	AWKWARD TO APPLY FULLY WITHOUT MOVING HAND ON CONTROL COLUMN.
32	1	WITH LOCK, KNOWS SOMETHING DIFFICULT TO UNLOCK. RUDDER ADJUSTMENT
33	1	AND EASE OF ADJUSTMENT EXCELLENT.
34	1	CANNOT REACH TO RELEASE - NEED ROPE! CANNOT REACH SWITCHES ON FWD
35	1	PANEL! TRIM CONTROL TIRING AND IRRITATING TO USE.

# SAILPLANE 4 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV	
9	B. PILOT OPINION OF COCKPIT LAYOUT	.00	.00	4.00	2.00	2.00	6.00	5.00	4.250	1.879	
10	1. PILOT COMFORT	.00	2.00	2.00	2.00	2.00	4.00	2.00	2.333	.745	
11	2. CONTROL SYSTEM ARRANGEMENT	.00	.00	2.00	2.00	2.00	5.00	7.00	4.000	1.600	
12	3. INSTRUMENT DISPLAY	.00	.00	3.00	1.00	2.00	3.00	3.00	2.000	.832	
13	4. PILOT VISIBILITY	.00	4.00	1.00	1.00	2.00	2.00	1.00	1.833	1.067	
14	5. PILOT SAFETY	.00	2.00	2.00	1.00	1.00	2.00	.00	1.600	.600	
75	AVER. AND STD. DEV. OF SUBTASKS(1:2...)	.0	.0	2.7	.9	2.1	1.7	1.6	.8	2.0	1.50

TASK	PILOT	COMMENTS
7	1	GOOD
8	1	COCKPIT IS SMALL. MY HEAD ALMOST TOUCHES THE CANOPY WHICH CAN LEAD
9	1	TO SOME BUMS IN TURBULENCE.
10	1	COMPLEX FLAP CONTROL. AWKWARD FOR 1.30RAD FLAP
11	1	FLAPS UNHANDY, COMPLICATED, EXCESSIVE FORCES, SUSCEPTIBLE TO MIS-USE
12	1	(SOARING FLAP NOT PUT UP BEFORE LANDING FLAP OPERATED)
13	1	FLAP HANDLE, TRIM HANDLE, AND BRAKE SHOULD BE IMPROVED
14	1	TRIM CONTROL IS TOO FAR FROM PILOT. FLAP CONTROL IS TOO COMPLICATED
15	1	AND FORCES ARE TOO HIGH AT MAX FLAP SPEEDS.
16	1	THE TRIM CONTROL IS A LITTLE AWKWARD TO REACH AND TO MOVE PRECISELY.
17	1	OPERATION OF FLAP HANDLE REQUIRES ABOUT 80-90% OF PILOT APPLICATION.
18	1	TO RELEASE NOT OBVIOUS. LOOKS LIKE AN AIRVENT.
19	1	THROUGHOUT NOT NEEDED.
20	1	WHILE VISIBILITY AND COMFORT ARE GOOD, THE COCKPIT LAYOUT AND HANDLES
21	1	ARE LESS THAN DESIRABLE. APPEARANCE IS POOR (INTERIOR)
22	1	WANT TO USE FULL LANDING FLAP POSITION DUE TO AWKWARD PLACEMENT
23	1	TRIM CONTROL TOO FAR FWD. ON TOW, BREAKOUT FORCE IN FWD. DIRECTION

\*\*\*\*\* ZEROS INDICATE NO RATING BY PILOT \*\*\*\*\*

# SAILPLANE 5 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV					
6	B. PILOT OPINION OF COCKPIT LAYOUT	2.50	2.00	2.00	.70	.00	1.00	1.00	1.700	.600					
7	1. PILOT COMFORT	.00	.00	.00	.00	.00	.00	.00	.000	.000					
8	2. CONTROL SYSTEM ARRANGEMENT	.00	.00	.00	.70	.00	.00	.00	.700	1.479					
9	3. INSTRUMENT DISPLAY	.00	.00	.00	.70	.00	.00	.00	.700	.490					
10	4. PILOT VISIBILITY	.00	.00	.00	.70	.00	.00	.00	.700	.894					
11	5. PILOT SAFETY	3.00	3.00	3.00	.00	.00	6.00	.00	3.750	1.299					
75	AVER. AND STD. DEV. OF SUBTASKS(EX 1:2:..)	2.2	1.0	2.2	.4	2.0	.6	.0	.0	3.4	1.9	1.0	.0	2.2	1.28

TASK	PILOT	COMMENTS
6	1	DRAW CHUTE DEPLOYMENT LEVER IN ANKWARD POSITION
7	1	CONTROL STICK AND RELEASE LEVER TOO FAR FWD
8	1	VERY UNCOMFORTABLE COCKPIT GENERALLY WELL LAID OUT. TRIMMER IS
9	1	HARD TO OPERATE AND HIGHLY ANNOYING. DRAW CHUTE KNOWN SUSCEPTIBLE
10	1	TO INADVERTENT OPERATION.
11	1	EXCELLENT COCKPIT LAYOUT
12	1	ELEVATOR OFFSET SO AS TO GIVE MOMENTUM TO UP ELEVATOR WHEN YOU HIT
13	1	A POSITIVE "TOY RELEASE TOO FAR FWD.
14	1	PILOT VISIBILITY MARGINAL DURING TOW
15	1	EXCELLENT
16	1	VIEW OF TOWPLANE OK, BUT COULD BE IMPROVED.
17	1	COCKPIT CONSTRUCTION MINIMAL IN STRENGTH
18	1	NOT AS SAFE AS SOME
19	1	EXCESSIVE BALLAST IN NOSE COULD BE CONVERTED INTO GLASS TO IMPROVE
20	1	PILOT'S PROTECTION
21	1	PILOT COMFORT IS EXCELLENT. VENTILATION SHOULD BE BETTER. VENT AIR
22	1	EXHAUST SHOULD HAVE BEEN PROVIDED.
23	1	EXCELLENT CONTROL PLACEMENT, SEAT DESIGN AND VISIBILITY. FLAP AND
24	1	SPEED BRAKE CONTROLS ARE WELL LOCATED AND CONVENIENT TO USE.

# SAILPLANE 6 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV						
6	B. PILOT OPINION OF COCKPIT LAYOUT	.00	.00	3.00	.00	.00	1.00	.00	2.000	1.000						
7	1. PILOT COMFORT	.00	.00	3.00	.00	.00	.00	.00	1.000	.745						
8	2. CONTROL SYSTEM ARRANGEMENT	.00	2.00	3.00	.00	.00	.00	.00	1.000	.745						
9	3. INSTRUMENT DISPLAY	.00	.00	3.00	.00	.00	.00	.00	1.000	.745						
10	4. PILOT VISIBILITY	.00	.00	3.00	.00	.00	.00	.00	1.000	.745						
11	5. PILOT SAFETY	.00	2.00	3.00	.00	.00	1.00	.00	1.000	.745						
75	AVER. AND STD. DEV. OF SUBTASKS(EX 1:2:..)	.0	.0	1.7	.4	2.0	.9	1.8	.7	1.6	.8	2.2	1.2	2.2	1.0	.94

TASK	PILOT	COMMENTS
7	2	EXCELLENT
8	2	TRIM WHEEL SHOULD BE ON LEFT
9	2	TRIM WHEEL LOCATED ON WRONG SIDE OF COCKPIT
10	2	STICK TOO FAR FWD. TRIM WHEEL ON WRONG SIDE.
11	2	TOY RELEASE SHOULD BE OFF TO LEFT SIDE. TRIM WHEEL ON LEFT SIDE
12	2	TRIM CONTROL SHOULD BE ON LEFT SIDE OF COCKPIT. STICK TOO FAR FWD
13	2	AT MOST FWD POSITION
14	2	FAIRLY POOR ON THIS GLIDER, SHOULD HAVE COMPENSATED VARIOMETERS
15	2	NON STANDARD
16	2	EXCELLENT
17	2	EXCELLENT
18	2	VERY SUBSTANTIAL COCKPIT STRUCTURE
19	2	TRIM WHEEL SIDE AND HARD TO USE
20	2	GOOD, SAFE DESIGN FEATURES IN COCKPIT. I WOULD QUESTION SOME OF THE
21	2	AERODYNAMIC COMPROMISES MADE FOR THE SAKE OF NOISINESS
22	2	CONTROL TRAVEL IS MUCH TOO EXTENSIVE FOR RUDDER, AILERON, ELEVATOR,
23	2	AND GIVE BRAKES

\*\*\*\*\* ZEROS INDICATE NO RATING BY PILOT \*\*\*\*\*

# SAILPLANE 1 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV
12	II. SMOOTH AIR MANEUVERING	1.50	1.00	1.00	.00	.00	1.00	.00	1.125	.217
13	A. PILOT OPIN OF INITIAL TAKEOFF RLL	1.00	1.00	1.00	.00	.00	1.00	.00	1.667	.943
14	1. TOW LINE HOOKUP	1.00	.00	1.00	.00	.00	1.00	.00	1.600	.690
15	2. CONTROL OF PLANE IN INIT. ROLL	1.00	1.00	1.00	2.00	4.50	1.00	2.00	1.786	1.191
76	AVER. AND STD. DEV. OF SUBTASKS(EX 1:2:..)	1.0	.0 1.0	.0 1.5	.5 2.0	.0 3.2	1.3 1.0	.0 2.0	.0 1.7	.97

TASK	PILOT	COMMENTS
76	3	EXCELLENT CHARACTERISTICS IN THIS PHASE OF THE FLIGHT
76	7	ON ONE TOW I HAD FULL FORWARD STICK AND WAS STILL GOING UP WHILE
76		TOW PLANE WAS STILL ON GROUND. PROBABLY SHOULD HAVE RELEASED.
76		NO PROBLEMS IN TAKE OFF, INCLUDING LIGHT CROSSWIND 9KTS, 45 DEG TO RWY

# SAILPLANE 2 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV
12	II. SMOOTH AIR MANEUVERING	2.00	2.00	3.00	.00	.00	2.00	3.00	2.400	.890
13	A. PILOT OPIN OF INITIAL TAKEOFF RLL	1.50	1.00	1.00	.00	.00	3.00	3.00	2.750	.900
14	1. TOW LINE HOOKUP	1.00	1.00	1.00	.00	.00	3.00	3.00	2.167	.847
15	2. CONTROL OF PLANE IN INIT. ROLL	2.00	1.00	1.00	4.00	4.00	4.00	2.00	3.143	.990
76	AVER. AND STD. DEV. OF SUBTASKS(EX 1:2:..)	1.5	.5 2.0	.0 3.0	1.0 4.0	.0 3.5	.5 3.5	.5 2.0	.0 2.7	.99

TASK	PILOT	COMMENTS
76	2	SOME TENDENCY TO DROP WING AT START. DON'T LIKE TO HAVE TO MOVE
76		FLAPS DURING T.O. ROLL (UP AT START, TO NEUTRAL) FLAP OPERATING
76		HANDLE EXCELLENT.
76		THERE IS A TENDENCY TO DROP A WING ON ROLLOUT. STICK LOCATION IS
76		INCONVENIENT.
76		INSUFFICIENT RUDDER, LOCATION OF CONTROL STICK, CONTROL STICK SHORT
76		TRAVEL, LACK OF CONTROL FORCES, AND LACK OF SAILPLANE 2 EXPERIENCE
76		RESULTED IN POOR T.O. CONTROL
76		WAS ALWAYS ALWAYS DRAGGED ON INITIAL ROLL, FELT LIKE NOT ENOUGH
76		WING TO STAY PULLED UP. STICK TOO FAR FORWARD
76		ALLTHOUGH IMPERFECTIVE AT FIRST EVEN WITH FLAPS IN THE NEGATIVE
76		NO PROBLEMS IN TAKEOFF, INCLUDING LIGHT CROSSWIND 19KTS, 785 RAD TO RW

\*\*\*\*\* ZEROS INDICATE NO RATING BY PILOT \*\*\*\*\*

# SAILPLANE 3 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV
12	II. SMOOTH AIR MANEUVERING	3.00	1.00	2.00	1.00	1.00	2.00	1.00	2.333	.571
13	A. PILOT OPIN OF INITIAL TAKEOFF RLL	1.00	3.00	1.00	2.00	1.00	1.00	1.00	1.571	.729
14	1. TOWLINE HOOKUP	1.00	2.00	1.00	1.00	1.00	1.00	1.00	1.333	.463
15	2. CONTROL OF PLANE IN INIT. ROLL	2.00	4.00	1.00	2.00	1.00	3.00	1.00	2.571	.729
76	AVER. AND STD. DEV. OF SUBTASKS(EX 1:2:..)	2.5	.5	3.0	1.0	1.5	.5	2.0	.0	.84

TASK	PILOT	COMMENTS
12	1	PILOT USUALLY PUMPS ELEVATOR
13	1	POOR LOCATION
14	1	PULLED ON ROPE EXTENSION BECAUSE HANDLE TOO FAR FWD.
15	1	VISIBILITY AND DIRECTIONAL CONTROL LIMITED
16	1	CROSS WIND CAPABILITY MARGINAL
17	1	6,7,9 DIVERGES; TOO DANGEROUS; EXTREME
18	1	RUDDER PEAK DURING ROLL. EASY TO DROP WING TO GROUND
19	1	NO PROBLEM WITH INITIAL TAKEOFF ROLL
20	1	ON TAKEOFF ROLL WITH AIR VENT OPEN; SAND AND ROCKS WERE BLOWN
21	1	THROUGH THE VENT INTO THE COCKPIT BY THE TOWPLANE.

# SAILPLANE 4 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV			
12	II. SMOOTH AIR MANEUVERING	.00	.00	.00	.00	.00	.00	.00	.000	.000			
13	A. PILOT OPIN OF INITIAL TAKEOFF RLL	.00	.00	.00	.00	.00	.00	.00	.000	1.000			
14	1. TOWLINE HOOKUP	.00	.00	.00	.00	.00	.00	.00	.000	.000			
15	2. CONTROL OF PLANE IN INIT. ROLL	.00	.00	.00	.00	.00	.00	.00	.000	.577			
76	AVER. AND STD. DEV. OF SUBTASKS(EX 1:2:..)	.0	.0	2.0	1.0	2.0	.0	1.0	.5	1.5	.5	1.6	.84

TASK	PILOT	COMMENTS
12	1	EXCELLENT AERODYNAMICALLY; CONFUSING FOR PILOT SINCE HE ALWAYS PULLS
13	1	RELEASE FOR HOOKUP.
14	1	GOOD
15	1	REQUIREMENT TO START T.O. WITH FLAP UP; THEN PUT NEUTRAL IS
16	1	UNDESIRABLE. SOME TENDENCY TO DROP WING AT START OF ROLL
17	1	MOST SERIOUS DEFICIENCY I NOTE IS THE SUDDEN BLOW TO THE TAILWHEEL
18	1	WHEN THE TAILWHEEL BECOMES TAUT
19	1	THERE IS ADEQUATE CONTROL DURING T.O. TO MAINTAIN WINGS LEVEL EVEN
20	1	IN CROSSWINDS OF AT LEAST 10KTS.
21	1	IS ABOUT TWICE THE AFT BREAKOUT FORCE. WHEN THE STICK IS MOVED AFT
22	1	TO FWD, THE FWD BREAKOUT FORCE IS RELATIVELY SO HEAVY THAT IT FEELS
23	1	AS IF A STOP HAS BEEN ENCOUNTERED. THIS UNBALANCED BREAKOUT FORCE
24	1	CAUSED ME TO OVERCONTROL IN PITCHDOWN ON ONE TAKEOFF. IT HAS BEEN
25	1	SUGGESTED (PILOT 4) THAT WITH LONGER TRIM CONTROL ALMOST FULL FWD.
26	1	(AS REGD ON TOW); BREAKOUT FORCES ARE UNEVEN FWD AND AFT AS AN
27	1	INHERENT CHARACTERISTIC OF THE FEEL SPRING MECHANISM.



\*\*\*\*\* ZEROS INDICATE NO RATING BY PILOT \*\*\*\*\*

#### SAILPLANE 5 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV
12	II. SMOOTH AIR MANEUVERING	.00	5.00	2.00	.00	.00	2.00	4.00	3.000	1.265
13	A. PILOT OPIN OF INITIAL TAKEOFF RLL	.00	4.00	1.00	.00	.00	3.00	3.00	2.200	1.160
14	1. TOWLINE HOOKUP	.00	4.00	1.00	.00	.00	3.00	3.00	2.200	1.160
15	2. CONTROL OF PLANE IN INIT. ROLL	.00	4.00	1.00	.00	.00	3.00	3.00	2.200	1.160
76	AVER. AND STD. DEV. OF SUBTASKS(EX 1,2,...)	2.5	.5	3.0	1.0	2.0	1.0	.0	.0	1.17

TASK	PILOT	COMMENTS
13	6	RUDDER INEFFECTIVE; FLAP/AILERON MOVEMENT NECESSARY TO CONTROL
14	6	WING LEVEL
15	6	POOR LOCATION
16	6	TOW RELEASE TOO FAR FROM PILOT'S SHOULDER. TOW HOOK TOO FAR AFT
17	6	CAUSING PITCHUP TENDENCY
18	6	VISIBILITY-DIRECTIONAL CONTROL LIMITED
19	6	AILERONS WEAK; RUDDER WEAK; LIMITED CROSSWIND CAPABILITY
20	6	THE USE OF UP-FLAP TO IMPROVE AILERONS IN CROSSWIND IS AN UNDESIRABLE
21	6	PROCEDURAL COMPLICATION. THE UNBALANCED LONGITUDINAL CONTROL
22	6	CIRCUIT CAUSES THE STICK TO BOUNCE FORE AND AFT WHILE ROLLING OVER
23	6	BUMPY GROUND
24	6	NO SIGNIFICANT PROBLEMS. SLIGHT BOUNCE ON TAKEOFF WHICH COULD BE
25	6	ATTRIBUTED TO WING FLEXING; PROBABLY IT WAS PILOT ERROR. IN ANY
26	6	CASE, AFTER LIFTOFF TOWPLANE SHOULD BE FOLLOWED HIGHER THAN WITH
27	6	OTHER SAILPLANES.
28	6	CROSSWINDS A MAJOR PROBLEM. MAX VECTOR PROBABLY ABOUT 15KNOTS.
29	6	NO PROBLEMS ON TAKEOFF(TEAMMAN TOW)

#### SAILPLANE 6 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV
12	II. SMOOTH AIR MANEUVERING	.00	1.00	1.00	.00	3.00	2.00	1.00	1.250	.933
13	A. PILOT OPIN OF INITIAL TAKEOFF RLL	.00	1.00	1.00	.00	3.00	2.00	1.00	1.250	.933
14	1. TOWLINE HOOKUP	.00	1.00	1.00	.00	3.00	2.00	1.00	1.250	.933
15	2. CONTROL OF PLANE IN INIT. ROLL	.00	1.00	1.00	.00	3.00	2.00	1.00	1.250	.933
76	AVER. AND STD. DEV. OF SUBTASKS(EX 1,2,...)	.0	.0	2.5	1.5	1.5	.5	1.0	.0	1.04

TASK	PILOT	COMMENTS
13	5	END STICK. ARM OUTSTRETCHED
14	5	EXCELLENT CONTROL DURING INITIAL ROLL AND LIFTOFF
15	5	VERY GOOD CONTROL IN ALL AXES FOR TAKEOFF-ADEQUATE AUTHORITY AND
16	5	RESPONSE.



# SAILPLANE 1 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV							
16	B. PILOT OPION OF TOW	1.50	1.00	2.00	2.00	3.00	1.00	1.00	1.375	.415							
17	1. EASE OF MAINTAINING POSITION	1.00	1.00	1.00	2.00	3.00	1.00	1.00	1.429	.728							
18	2. AIRCRAFT TRIM	2.00	5.00	1.00	2.00	3.00	4.00	4.00	1.500	1.336							
19	3. CONTROL IN PROWASH	1.00	1.00	1.00	2.00	3.00	1.00	1.00	1.429	.728							
20	4. RELEASE CHARACTERISTICS	1.00	.00	2.00	1.00	2.00	1.00	2.00	1.500	.500							
77	AVER. AND STD. DEV. OF SUBTASKS(EX 1,2,...)	1.3	.4	2.3	1.9	1.3	.4	2.2	1.1	3.1	.9	1.7	1.3	2.0	1.2	2.0	1.27

TASK	PILOT	COMMENTS
17	6	INSUFFICIENT ELEVATOR TRIM. REQUIRES ABOUT 13N CONSTANT PUSH FORCE
18	6	HEADING DOES NOT HUNT. EXCELLENT FOLLOWING OF TOWPLANE.
19	6	TOO MUCH FORWARD STICK TO MAINTAIN POSITION
20	6	INEFFECTIVE-UNSATISFACTORY
21	6	POOR NONEXISTENT
22	6	MAX TRIM SPEED 45-50KTS, HOWEVER FORCES ARE LIGHT THROUGH SPEED RANGE
23	6	EXCELLENT
24	6	EXTREMELY RESPONSIVE--WELL DAMPED--LIGHT CONTROL FORCES
25	6	GOOD HARMONY--OUTSTANDING
26	6	SLIDER CANNOT BE TRIMMED ON TOW. WOULD BE TIRESOME AS A CROSS-COUNTRY
27	6	TOW
28	6	CONSTANT FORWARD FORCE ON STICK
29	6	TRIM-REQUIRED 13-18N FWD FORCE IN TOW. CONTROL VERY GOOD IN TOW.
30	6	BOXING SAILPLANE IS SIMPLE TASK; WINGS LEVEL(ADEQUATE RUDDER CONTROL)

# SAILPLANE 2 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV					
16	B. PILOT OPION OF TOW	1.00	2.00	3.00	2.00	3.00	3.00	3.00	2.200	.748					
17	1. EASE OF MAINTAINING POSITION	1.00	3.00	3.00	2.00	3.00	3.00	3.00	2.500	.700					
18	2. AIRCRAFT TRIM	1.00	3.00	3.00	2.00	3.00	3.00	3.00	2.571	.728					
19	3. CONTROL IN PROWASH	1.00	2.00	3.00	2.00	3.00	3.00	3.00	2.143	.639					
20	4. RELEASE CHARACTERISTICS	1.00	.00	3.00	1.00	2.00	3.00	3.00	1.667	.471					
77	AVER. AND STD. DEV. OF SUBTASKS(EX 1,2,...)	1.0	.0	2.3	.5	2.5	.4	2.2	.4	2.7	.4	2.2	.4	2.2	.72

TASK	PILOT	COMMENTS
17	6	INSUFFICIENT RUDDER TO BOX TOWPLANE
18	6	EFFECTIVE BUT HARD TO OPERATE
19	6	FRICTION FORCE IS SUFFICIENT
20	6	SUFFICIENT TRIM AVAILABLE HOWEVER EACH DETENT RESULTED IN AT LEAST
21	6	8X1 INCREMENTS
22	6	DIRECTIONAL-COULD NOT BOX TOW VERY WELL
23	6	FAIRLY LARGE AILERON DEFLECTIONS ARE REQUIRED.
24	6	ALWAYS NEED PUSH FORCES ON STICK
25	6	GOOD, QUIET
26	6	TOUCHY IN DIRECTIONAL
27	6	SOME CONCENTRATION REQUIRED FOR DIRECTIONAL-LATERAL CONTROL
28	6	HANDLES EXCELLENTLY. EASILY UPSET BY DRAUGHTS BUT EASILY RESTORED
29	6	BY CONTROLS
30	6	PLEASANT LIGHT RUDDER FORCES. GEAR RETRACTION FORCES ARE HEAVY,
31	6	UNCOMFORTABLE. SLIGHT OVERSHOOT WHEN MOVING BACK TO CENTER FROM
32	6	THE OUTSIDE. CURIOUS CLIPPING NOISE COMING FROM THE REAR IN THE
33	6	RUDDER CIRCUIT. UNPLEASANT STICK FORCES, EXCESSIVE FRICTION. POOR
34	6	VISIBILITY
35	6	DIFFICULT TO FLY WAS IN ROUGH AIR. HAD TO WORK TO RETURN TO CORRECT
36	6	POSITION.
37	6	NON-STANDARD STICK TOO FAR FORWARD RESULTING IN TROUBLE HOLDING
38	6	WING DOWN AT HIGH TOW SPEEDS.
39	6	ADEQUATE RUDDER CONTROL TO BOX TOWPLANE WITH WINGS LEVEL. SMALL BIT
40	6	PRELUENT STICK AND RUDDER INPUTS REQUIRED IN NORMAL TOW.

\*\*\*\*\* ZEROS INDICATE NO RATING BY PILOT \*\*\*\*\*

# SAILPLANE 3 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV					
16	B. PILOT OPTION OF TOW	2.00	3.00	2.00	3.00	2.00	3.00	2.00	2.500	.500					
17	1. EASE OF MAINTAINING POSITION	2.00	2.00	2.00	3.00	2.00	3.00	2.00	2.286	.700					
18	2. AIRCRAFT TRIM	3.00	2.00	2.00	3.00	2.00	3.00	2.00	2.429	.445					
19	3. CONTROL IN PROPWASH	1.00	2.00	3.00	3.00	2.00	3.00	2.00	1.857	.634					
20	4. RELEASE CHARACTERISTICS	1.00	.00	3.00	3.00	2.00	3.00	2.00	2.143	.687					
77	AVER. AND STD. DEV. OF SUBTASKS(EX 1:2+...)	1.7	.8	2.0	.0	2.2	.4	2.5	.0	2.5	.5	1.7	.4	2.2	.67

TASK	PILOT	COMMENTS
17	1	FWD VISIBILITY LIMITED
17	1	EASY TO MAINTAIN POSITION
17	1	THERE WAS SOME VERTICAL OSCILLATION EACH TIME THERE WAS A SLACK ROPE
17	1	AND THE TOWPLANE TOOK UP THE SLACK. I BELIEVE THIS WAS MORE
17	1	PRONOUNCED BECAUSE OF TOW ROPE HOOKUP LOCATION
17	1	COULD NOT BOX TOWPLANE IN LOW POSITION DUE TO TOWLINE RUB ON FUSELAGE
17	1	BOTTOM
17	1	OVER SENSITIVE LONGITUDINAL CONTROL
17	1	IT CAN BE TRIMMED FOR LONG TOWS
17	1	ADEQUATE, HOWEVER, SOME DIFFICULTY IN ACTUATING TRIM LOCK.
17	1	CONTROL GOOD BUT TOWROPE RUBS SIDE OF FUSELAGE DUE TO LOCATION OF
17	1	RELEASE HOOK
17	1	NO PROBLEM
17	1	DID NOT CHECK BECAUSE OF TOW ROPE HOOKUP LOCATION
17	1	NOISY
17	1	ELEVATOR CONTROL FORCES NEGLECTIBLE, WHEN PULLED UP AND PUSHED OVER,
17	1	ENCOUNTERED NEGATIVE FC, COULD BE CORRECTED BY THE PILOT BEING
17	1	EXTREMELY LIGHT ON THE CONTROLS OR BY ELIMINATING THE PULLUP-PUSHOVER
17	1	PRIOR TO RELEASE.
17	1	NO COMMENTS, VERY GOOD
17	1	EASY TO OVERCONTROL IN PITCH
17	1	SOLID FEEL, GEAR RETRACTION MORE COMFORTABLE THAN SAILPLANE 2. TOW L
17	1	COMES UP SIDE OF FUSELAGE WHEN BOXING TOWPLANE.
17	1	HELD SAILPLANE OFFSET TO RIGHT SO I COULD SEE AROUND GLARE SHIELD!
17	1	WITH TOWPLANE CENTERED, HAD TO FLY LOW TO SEE OVER SHIELD.
17	1	WITHOUT USE OF RUDDER, NOSE WANDERS ABOUT 3/4 TOWPLANE SPAN. NO PROB.

# SAILPLANE 4 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV							
16	B. PILOT OPTION OF TOW	.00	2.00	3.00	2.00	2.00	2.00	2.00	2.200	.400							
17	1. EASE OF MAINTAINING POSITION	.00	2.00	2.00	3.00	2.00	2.00	2.00	2.000	.000							
18	2. AIRCRAFT TRIM	.00	1.00	2.00	3.00	2.00	2.00	2.00	1.500	1.250							
19	3. CONTROL IN PROPWASH	.00	2.00	3.00	3.00	2.00	2.00	2.00	2.167	.573							
20	4. RELEASE CHARACTERISTICS	.00	.00	3.00	3.00	2.00	2.00	2.00	1.800	.748							
77	AVER. AND STD. DEV. OF SUBTASKS(EX 1:2+...)	.0	.0	1.7	.5	3.0	.7	2.0	.7	1.7	.4	2.5	.9	1.7	.4	2.1	.80

TASK	PILOT	COMMENTS
17	3	THIS SAILPLANE WAS EASY TO LOCK IN POSITION.
17	3	CENTERING SPRING IS ANNOYING
17	3	ADEQUATE BUT DIFFICULT TO ACTUATE TRIM LEVER TO OBTAIN PRECISE
17	3	SETTINGS AND LEVER LOCATED TOO FAR FROM PILOT.
17	3	THE TRIM WAS VERY GOOD
17	3	EXCELLENT BUT NOISY
17	3	FELT SOLID, NOTED DURING TOW THAT NOSE UP BREAKOUT FORCE LESS THAN
17	3	NOSE DOWN. NOSE DOWN FELT LIKE A [STOP].
17	3	NOISY
17	3	GOOD
17	3	HANDLING DURING TOW IS GOOD, ONLY ANNOYING CHARACTERISTIC IS NOISE
17	3	STRONG POSITIVE TRIM FORCE CAUSES UNWANTED PITCH CHANGES(ATTITUDE)
17	3	ON TOW WHEN HITTING A BUST WHICH INCREASES/DECREASES AIRSPEED.
17	3	RUDDER CONTROL MORE THAN ADEQUATE TO MAINTAIN WING SEMISPAN LATERAL
17	3	OFFSET FROM TOWPLANE WITH WINGS LEVEL

\*\*\*\*\* ZEROS INDICATE NO RATING BY PILOT \*\*\*\*\*

# SAILPLANE 5 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV						
16	B. PILOT OPTION OF TOW	2.00	4.50	2.00	.00	.00	4.00	5.00	3.500	1.265						
17	1. EASE OF MAINTAINING POSITION	1.00	3.00	2.00	.00	.00	4.00	5.00	3.800	1.329						
18	2. AIRCRAFT TRIM	2.00	2.00	2.00	.00	.00	4.00	5.00	3.200	1.400						
19	3. CONTROL IN PROPWASH	1.00	2.00	.00	.00	.00	4.00	4.00	1.500	1.118						
20	4. RELEASE CHARACTERISTICS	1.00	.00	2.00	.00	.00	2.00	2.00	1.750	.433						
77	AVER. AND STD. DEV. OF SUBTASKS(EX 1:2:..)	1.3	.4	2.3	.5	2.0	.0	.0	.0	.0	2.7	.4	3.2	1.3	2.3	1.00

TASK	PILOT	COMMENTS
17	1	FWD VISIBILITY LIMITED
18	1	TRIMMED ON TOW
19	1	CONTROL GOOD BUT TOWROPE RUBS SIDE OF FUSELAGE DUE TO POS OF RELEASE
19	1	I FELT THAT, IN TURBULENCE, I WAS FAIRLY CLOSE TO A SERIOUS PITCH
19	1	CONTROL PROBLEM AT TIMES(PILOT INDUCED OSCILLATION). I WAS UNABLE
19	1	(AND UNWILLING TO TRY A SECOND TIME) TO RAISE THE LANDING GEAR WITH
19	1	THE RIGHT HAND WHILE FLYING WITH THE LEFT HAND, EVEN IN SMOOTH A/P.
19	1	AS USUAL WITH A VERY SENSITIVE PITCH CONTROL, I WAS VERY CONSCIOUS
19	1	THAT INPUTS AND CORRECTIONS MUST BE KEPT SMALL; THAT LARGE INPUTS
19	1	WOULD BE UNPLEASANT, IF NOT DOWNRIGHT HAIRY.
19	1	TOWS OK AT 70 KTS. AT 80 KTS THE NEGATIVE STICK FORCE/ICE GIVES
19	1	THE IMPRESSION OF HAVING A NEGATIVE(UNSTABLE) STICK FORCE GRADIENT.
19	1	THE STICK MUST BE RESTRAINED IN CENTER POSITION, MOST UNPLEASANT
19	1	ON TOW WHERE PITCH STEERING TASK IS TIGHTER.
19	1	INITIAL TOW SPEED 60KTS. FELT MORE COMFORTABLE WITH ONE NOTCH DOWN
19	1	FLAPS. NO BOXING OF TOWPLANE WAS ATTEMPTED. VERY EASY TO STAY IN
19	1	POSITION.
19	1	WITHOUT FEET ON RUDDER PEDALS, YAWS ABOUT ONE WING SPAN TO EITHER
19	1	SIDE OF TOWPLANE. CONTROLLABLE WITH RUDDER.
19	1	POOR HARMONY! VERY SENSITIVE ELEVATOR WITH RELATIVELY HEAVY,
19	1	SLUGGISH AILERONS. BOXING TOW TO SIDE WITH FULL RUDDER, WINGS LEVEL
19	1	ABOUT 1/2 SEMISPAN FROM TOWPLANE

# SAILPLANE 6 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV							
16	B. PILOT OPTION OF TOW	.00	1.00	2.00	1.00	.00	2.00	1.00	1.500	.500							
17	1. EASE OF MAINTAINING POSITION	.00	1.00	2.00	1.00	.00	2.00	1.00	1.667	.745							
18	2. AIRCRAFT TRIM	.00	.00	2.00	2.00	.00	2.00	1.00	2.000	1.020							
19	3. CONTROL IN PROPWASH	.00	1.00	1.00	2.00	.00	2.00	1.00	1.000	1.000							
20	4. RELEASE CHARACTERISTICS	.00	1.00	3.00	1.00	.00	2.00	2.00	1.833	.687							
77	AVER. AND STD. DEV. OF SUBTASKS(EX 1:2:..)	.0	.0	1.0	.0	2.0	.7	1.5	.4	2.5	.5	2.5	.9	2.0	1.2	2.0	.91

TASK	PILOT	COMMENTS
17	1	EXCELLENT
17	1	FWD STICK, ARM OUTSTRETCHED
18	1	GOOD
18	1	NOT ENOUGH NOSE DOWN TRIM
18	1	YRIM MAX 65IAS WITH SINGLE PILOT
19	1	BETTER THAN MOST
19	1	NOISY
19	1	EXTREMELY EASY TO TOW. AILERONS OSCILLATE OSCASIONALLY IN PROPWASH
19	1	OR TURBULENCE--THIS MIGHT ALARM STUDENT
19	1	VERY GOOD TOW CHARACTERISTICS, NOISIER THAN OTHERS.
19	1	RUDDER FORCE TOO HIGH FOR GOOD HARMONY
19	1	UNABLE TO TRIM OUT PITCHUP--HAD TO HOLD FWD FORCE CONTINOUSLY. VERY
19	1	GOOD IN HOLDING STABLE TOW POSITION, HOWEVER.

\*\*\*\*\* ZEROS INDICATE NO RATING BY PILOT \*\*\*\*\*

# SAILPLANE 1 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER. STD DEV
21	C. PILOT OPIN OF LONG. HANDLING	2.00	1.00	1.00	3.00	3.00	1.00	1.00	.250 .433
22	1. EASE OF EST & MAIN COM AIRSPEED	2.00	1.00	1.00	3.00	3.00	1.00	1.00	.250 .433
23	2. PLANE TRIM SYS OVER SPEED RANGE	2.00	1.00	1.00	3.00	3.00	1.00	1.00	.250 .433
24	3. PITCH SENSITIVITY	2.00	1.00	1.00	3.00	3.00	1.00	1.00	.250 .433
25	4. STICK FORCE GRADIENT	2.00	1.00	1.00	3.00	3.00	1.00	1.00	.250 .433
26	5. STICK FREE STABILITY	2.00	1.00	1.00	3.00	3.00	1.00	1.00	.250 .433
27	6. STICK FREE STABILITY	2.00	1.00	1.00	3.00	3.00	1.00	1.00	.250 .433
28	7. RETURN TO TRIM	2.00	1.00	1.00	3.00	3.00	1.00	1.00	.250 .433
29	8. MANEUVERING RESPSE	2.00	1.00	1.00	3.00	3.00	1.00	1.00	.250 .433
30	9. PHUGOID CHARACTERISTICS	2.00	1.00	1.00	3.00	3.00	1.00	1.00	.250 .433
31	10. DIVE RECOVERY	2.00	2.00	1.00	3.00	3.00	1.00	2.00	.250 .433
78	AVER. AND STD. DEV. OF SUBTASKS(EX 1,2,...)	1.5	.8	1.6	1.3	1.6	.7	1.6	1.1 2.3 .6 1.6 1.0 2.1 .8 1.7 .96

TASK	PILOT	COMMENTS
21	1	EASY TO OBTAIN, BUT HAD TO HOLD A FORCE AT SPEEDS ABOVE 48KTS.
22	1	VERY EASY TASK
23	1	TRIMMER UNSATISFACTORY
24	1	NOT NEEDED
25	1	MAX TRIM SPEED 48KTS.
26	1	COULD ONLY TRIM TO 61 IAS
27	1	INSUFFICIENT NOSE DOWN TRIM FOR MAX AIRSPEED
28	1	STEADY STATE SPEED WITH FULL FWD TRIM AT 55KTS-NEEDS FULL TRIM CAP.
29	1	EXCELLENT
30	1	NO PROBLEMS AT ALL IN OVER 161 OR UNDESIRABLE RESPONSE
31	1	EXCELLENT
32	1	LIGHT BUT GOOD-RARELY BOTHER TRIMMING WHILE SOARING
33	1	VERY GOOD
34	1	TRIMMER INOPERATIVE
35	1	VERY GOOD
36	1	TRIMMER INOPERATIVE BUT PROBABLY WOULD RETURN TO TRIM
37	1	RAN OUT OF TRIM
38	1	EXCELLENT
39	1	NEUTRALLY STABLE AT 52KTS
40	1	NEUTRAL
41	1	NEUTRAL
42	1	A LITTLE TOO LIGHT STABILITY CAUSES 6 TO BUILDUP DURING DIVE ACCEL.
43	1	MODERATE STICK FORCE REQUIRED
44	1	IS-18N IN TURNING FLIGHT AT 52KTS POSITIVE AND OK
45	1	STABILITY INDICED 6 DURING DIVE RECOVERY LEADS TO EASE OF OVER 6
46	1	EXCELLENT LONGITUDINAL STABILITY, VERY PERCEPTIBLE STICK TRAVEL AND
47	1	FORCE REQUIRED FOR SPEED CHANGE, NON LINEAR RESPONSE DURING PRECISE
48	1	ATTITUDE CHANGE(SLOWER RESPONSE TO PUSH THAN TO PULL).
49	1	STICK FORCE PER 1% EXCELLENT
50	1	STICK VERY FORWARD
51	1	PITCH-ROLL CONTROL AND RESPONSE HARMONY IS VERY GOOD

\*\*\*\*\* ZEROS INDICATE NO RATING BY PILOT \*\*\*\*\*

# SAILPLANE 2 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV							
2	C. PILOT OPIN OF LONG. HANDLING	3.00	2.00	3.00	3.00	3.00	3.00	3.00	2.600	.800							
3	1. EASE OF EST & MAIN CON AIRSPEED	3.00	2.00	3.00	3.00	3.00	3.00	3.00	2.629	.728							
4	2. PLANE TRIM SYS OVER SPEED RANGE	3.00	2.00	3.00	3.00	3.00	3.00	3.00	2.629	.728							
5	3. PITCH SENSITIVITY	3.00	2.00	3.00	3.00	3.00	3.00	3.00	2.629	.728							
6	4. STICK FORCE GRADIENT	3.00	2.00	3.00	3.00	3.00	3.00	3.00	2.629	.728							
7	5. STICK FIXED STABILITY	3.00	2.00	3.00	3.00	3.00	3.00	3.00	2.629	.728							
8	6. STICK FREE STABILITY	3.00	2.00	3.00	3.00	3.00	3.00	3.00	2.629	.728							
9	7. RETURN TO TRIM	3.00	2.00	3.00	3.00	3.00	3.00	3.00	2.629	.728							
10	8. MANEUVERING RESPSE	3.00	2.00	3.00	3.00	3.00	3.00	3.00	2.629	.728							
11	9. PHUGOID CHARACTERISTICS	3.00	2.00	3.00	3.00	3.00	3.00	3.00	2.629	.728							
12	10. DIVE RECOVERY	3.00	2.00	3.00	3.00	3.00	3.00	3.00	2.629	.728							
78	AVER. AND STD. DEV. OF SUBTASKS (EX 1:2+...)	2.7	1.3	1.9	.0	2.8	.6	2.3	.8	2.6	.7	2.6	.7	2.0	.7	2.6	.89

TASK	PILOT	COMMENTS
1	1	POORER THAN SOME SAILPLANES
2	1	DIFFICULT TO OBTAIN PRECISE TRIM SPEEDS
3	1	TRIM
4	1	GOOD, BUT MINIMUM INCREMENT TOO LARGE
5	1	POOR TRIM, NOT REALLY NEEDED
6	1	TRIM WAS ADEQUATE IF PRECISE TRIM SPEEDS ARE NOT REQUIRED.
7	1	MORE SENSITIVE THAN OTHERS
8	1	VERY SENSITIVE BUT LACK OF FORCE GRADIENT CAUSES SOME DIFFICULTY
9	1	IN OBTAINING PRECISE PITCH INPUTS
10	1	WIDE FRICTION BAND
11	1	VERY LIGHT FORCE GRADIENT. ALMOST NEUTRAL STATIC LONG. STAB.
12	1	ON
13	1	STABLE FORCE BUT VERY LIGHT
14	1	FORCES VERY LOW, BUT JUST PERCEPTIBLE
15	1	BARELY PERCEPTIBLE GRADIENT
16	1	NOT CHECKED
17	1	NOT POSSIBLE BECAUSE OF WIDE FRICTION BAND
18	1	VERY GOOD WHEN A/S WAS DISPLACED TO THE HIGH SIDE. VERY POOR WHEN
19	1	A/S WAS DISPLACED TO THE LOW SIDE.
20	1	DOES NOT RETURN, BUT WHO CARES.
21	1	VTRIM 57IAS DFLAP=0-LOW 49 HIGH 74; VTRIM 50 DFLAP=1, LOW 46 HIGH 80
22	1	VTRIM 71IAS DFLAP=1 LOW 58 HIGH 85
23	1	FLEXIBLE WING GIVES SPONGY FEEL
24	1	SENSITIVE
25	1	NO FORCE GRADIENT
26	1	HAVE TO WORK AT COORDINATION; RUDDER WEAK
27	1	LIGHTLY DAMPED
28	1	VERY DAMPED PHUGOID
29	1	CURING 1ST FLIGHT DIVERGENT AT HIGHER SPEED. 2ND FLT. NEUTRAL TO
30	1	SLIGHTLY POSITIVE AT TRIM A/S 54 AND 70KTS.
31	1	UNPREDICTABLE; LONG PERIOD; DANGEROUS SOMETIMES, SOMETIMES NEUTRAL
32	1	OR DIVERGE
33	1	SLIGHTLY DIVERGENT
34	1	VTRIM 54IAS PERIOD 28SEC, VTRIM 70IAS PERIOD 46SEC LIGHTLY DAMPED
35	1	VERY LIGHT APPROX 4.5-ON/G
36	1	NO FORCE GRADIENT
37	1	ACCELERATES VERY RAPIDLY WITH NOSE DOWN
38	1	6:7:9 UNDESIRABLE AT HIGH SPEEDS BECAUSE OF DIVERGENCE--NEUTRAL
39	1	AT SPEEDS UP TO 57-61 IAS.
40	1	SENSITIVE IN PITCH; VERY SMALL STICK MOVEMENTS NEEDED TO MAKE PRECISE
41	1	ATTITUDE CHANGES. TRIM WAS SET AT 5TH NOTCH FROM REAR AND LEFT
42	1	THREAT FOR MOST OF FLIGHT.
43	1	VERY LIGHT STICK FORCES--VERY LIGHT GRADIENT--OK

\*\*\*\*\* ZEROS INDICATE NO RATING BY PILOT \*\*\*\*\*

# SAILPLANE 3 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVGR.	STD DEV							
21	C. PILOT OPIN OF LONG. HANDLING	5.00	5.00	2.50	3.20	2.00	3.00	3.00	2.100	1.118							
22	1. EASE OF EST & MAIN CON AIRSPEED	2.00	2.00	2.00	3.00	2.00	3.00	3.00	2.246	1.452							
23	2. PLANE TRIM SYS OVER SPEED RANGE	2.00	2.00	2.00	3.00	2.00	3.00	3.00	2.355	1.247							
24	3. STICK SENSITIVITY	2.00	2.00	2.00	3.00	2.00	3.00	3.00	2.714	1.700							
25	4. STICK FORCE GRADIENT	2.00	2.00	2.00	3.00	2.00	3.00	3.00	2.286	1.030							
26	5. STICK FIXED STABILITY	2.00	2.00	2.00	3.00	2.00	3.00	3.00	2.950	1.433							
27	6. STICK FREE STABILITY	2.00	2.00	2.00	3.00	2.00	3.00	3.00	3.424	2.770							
28	7. RETURN TO TRIM	2.00	2.00	2.00	3.00	2.00	3.00	3.00	3.800	3.187							
29	8. MANEUVERING RESPSE	2.00	2.00	2.00	3.00	2.00	3.00	3.00	2.714	1.881							
30	9. PHUGOID CHARACTERISTICS	2.00	2.00	2.00	3.00	2.00	3.00	3.00	2.286	2.603							
31	10. DIVE RECOVERY	2.00	2.00	2.00	3.00	2.00	3.00	3.00	2.000	2.000							
78	AVGR. AND STD. DEV. OF SUBTASKS(EX 1:2+...)	4.4	3.7	3.1	1.5	2.5	.5	2.7	2.1	3.6	1.4	3.2	.7	2.4	.4	3.1	2.05

TASK	PILOT	COMMENTS
21	21	POOR OPERATING DEVICE
22	22	DURING DESCENT AND TRIMMING AT 60IAS AND HOLDING ELEVATOR CONTROL
23	23	FIXED-NOTED A +-1 KT OSCILLATION. SPEED VARIATION WAS CONFIRMED
24	24	BY NOTING SLIGHT A/C OSCILLATION.
25	25	VTRIM SORTS FRICTION BAND LOW 42 HIGH 53. VTRIM 60KTS LOW 48 HIGH 68
26	26	VTRIM 70KTS LOW 57 HIGH 73
27	27	SHIP GAINERS SPEED QUICKLY. EASY TO MAINTAIN SPEED.
28	28	50 TO 90 IAS
29	29	THIS IS FUNNY, BECAUSE IT FEELS GOOD, BUT CAN'T TAKE HAND OFF FOR LONG
30	30	UNABLE TO TRIM HIGH ENOUGH SPEED. TRIM STOPS ABOUT 80IAS.
31	31	TOO SENSITIVE
32	32	FAIRLY SENSITIVE
33	33	VERY SENSITIVE, BUT LACK OF FORCE GRADIENT CAUSED SOME DIFFICULTY
34	34	IN OBTAINING PRECISE PITCH INPUTS
35	35	EASY TO OVERCONTROL AT HIGH SPEED.
36	36	SENSITIVE BUT NO OVER ICG PROBLEMS.
37	37	LIGHT STICK FORCES NOT UNPLEASANT
38	38	GRADIENT VERY LIGHT
39	39	BARELY PERCEPTIBLE
40	40	GOOD IN SPEED UP. POOR IN BELOW TRIM SPEED.
41	41	LIGHT BUT PERCEPTIBLE
42	42	INSENSITIVE AT LOW SPEED
43	43	FAIRLY GOOD
44	44	SPEED VS. POSITION GOOD.
45	45	NICE
46	46	LOWER THAN MOST. LOW FORCE GRADIENT
47	47	FORCES ARE VERY LOW BUT PERCEPTIBLE
48	48	BARELY PERCEPTIBLE
49	49	NOT CHECKED
50	50	NO RETURN TO TRIM
51	51	FROM HIGH SIDE (90 TO TRIM) GOOD. FROM LOW SIDE (49-69) POOR. BECAUSE
52	52	OF LOW FORCE GRADIENT.
53	53	SENSITIVE
54	54	STICK FORCE/ICG NEUTRAL
55	55	UNSATISFACTORY
56	56	AT 60IAS, PHUGOID QUICKLY DIVERGES. AT 80IAS ALMOST NEUTRALLY STABLE
57	57	TRIM 60 IAS NEUTRAL. TRIM AT 90 IAS DIVERGENT.
58	58	DIVERGENT VARIOUSLY AFTER 1/2 CYCLE (1IN PITCH)
59	59	DIVERGENT STRONGLY - PERIOD 18SEC AT VTRIM 50 KTS.
60	60	UNSATISFACTORY SLIGHTLY NEGATIVE STICK FORCE/ICG
61	61	NO PROBLEM
62	62	VERY SHARP FORCE ABRUPTLY APPLIED TO THE CONTROL. STICK RESULTED IN A
63	63	VERY SHARP PITCH UP. WHEN FORCE WAS RELEASED, ELEVATOR CONTROL
64	64	CONTINUED TO MOVE APT LIKE ELEVATOR OVER BALANCE) RESULTING IN
65	65	MORE PITCH UP. I THINK PULL UP ELEVATOR WOULD HAVE RESULTED IF I
66	66	HAD NOT RESTRAINED THE STICK MOVEMENT. THIS CONDITION IS NOT GOOD.
67	67	CAN'T LEV 60 OF STICK ABOVE 70IAS. WILL DIVERGE. NOT NEARLY AS
68	68	UNPLEASANT IN MANEUVERS AS SAILPLANE 5.
69	69	CONTROL STICK FEELS A LITTLE LOOSE. VERY LOW FORCE LEVELS. WHEN
70	70	STICK IS TAPPED FORWARD AT 80IAS, GLIDER NOSE SEEMS TO TUCK UNDER.
71	71	I BELIEVE THE TRUE PHUGOID WOULD HAVE TO BE OBSERVED STICK FIXED.
72	72	I THINK I9) IS A RESULT OF ELEVATOR FLOATING TO AUGMENT PHUGOID.
73	73	STICK FORCE/ICG VERY LIGHT AT 800G BANK. NEUTRAL AT 800G BANK.
74	74	HAS TRIMMED SPEED 92 KTS. CONTROL SYSTEM FRICTION VERY LOW (GOOD).

\*\*\*\*\* ZEROS INDICATE NO RATING BY PILOT \*\*\*\*\*

# SAILPLANE & DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV							
21	C. PILOT OPIN OF LONG. HANDLING	.00	.00	.00	.70	.00	.00	.00	3.200	.788							
22	1. EASE OF SET & MAIN COIL AIRSPEED	.00	.00	.00	.70	.00	.00	.00	.000	.000							
23	2. HOLD TRIM 5% OVER SPEED RANGE	.00	.00	.00	.70	.00	.00	.00	.000	.000							
24	3. STICK SENSITIVITY	.00	.00	.00	.70	.00	.00	.00	.000	.000							
25	4. STICK FORCE GRADIENT	.00	.00	.00	.70	.00	.00	.00	.000	.000							
26	5. STICK FIXED STABILITY	.00	.00	.00	.70	.00	.00	.00	.000	.000							
27	6. STICK FREE STABILITY	.00	.00	.00	.70	.00	.00	.00	.000	.000							
28	7. RETURN TO TRIM	.00	.00	.00	.70	.00	.00	.00	.000	.000							
29	8. MANEUVERING RESPCE	.00	.00	.00	.70	.00	.00	.00	.000	.000							
30	9. PHUGOID CHARACTERISTICS	.00	.00	.00	.70	.00	.00	.00	.000	.000							
31	10. DIVE RECOVERY	.00	.00	.00	.70	.00	.00	.00	.000	.000							
70	AVER. AND STD. DEV. OF SUBTASKS(EX 1+2+...)	.0	.0	2.1	.7	2.6	.8	1.6	.7	2.2	.6	2.9	1.0	2.2	.6	2.3	.87

TASK	PILOT	COMMENTS
1	1	OCCASIONAL OVERSHOOT IS EXPERIENCED WHEN CHANGES ARE ATTEMPTED TAS EASY TO OBTAIN; HOWEVER, IT IS DIFFICULT TO ACTUATE TRIM LEVER FOR MAINTAINING TAS HAND TO ADJUST PRECISELY ABLE TO TRIM THROUGHOUT REGD TO:M RANGE VERY GOOD VERY SENSITIVE FOUND CENTERING SPRING ANNOYING FORCE GRADIENT IS THE RESULT OF WORKING AGAINST SPRINGS. THIS RESULTS IN FORCES AS HIGH AS 19-22N. DURING ALL MANEUVERS EXCEPT T.O., LANDING, AND STICK FORCE/GR. VERY LIGHT FORCES WOULD BE MORE DESIRABLE. LIGHT BUT OK NON-LINEARITY OBSERVED GOING BACK FROM 57 TO 52 OK. STARTING FROM 48 OSCILLATION BEGAN. SAME AS STICK FIXED POSITIVE STICK FORCE/V GRADIENT DID NOT DO GOOD VERY PLEASANT IF SAME TRIM SPEED IS DESIRED AT END OF MANEUVER POSITIVE FORCE GRADIENT WITH GR. OK NEUTRAL VIBRATION NEUTRAL--APPROX. 16SEC PERIOD VIBRATION 40IAS 20 SEC PERIOD MODERATELY DAMPED LIGHT BUT NO SURPRISES GOOD NO PROBLEM POSITIVE FORCE GRADIENT WITH GR. GIVES IMPRESSION OF LIGHT STABILITY WITH STIFF, INSENSITIVE STICK. QUICK, LIGHT BUT CONSISTENT. PLEASANT TO FLY WHEN RETURNING FROM OFF TRIM CONDITION, PHUGOID OSCILLATION WAS NOTED IN 2 OF 3 CASES. STICK FORCE PER GR TOO LIGHT. STICK FORCE PER DISPLACEMENT MAY BE OK. STICK FORCE GRADIENT PER AIRSPEED TOO HIGH. HIGH STICK FORCE GRADIENT IN BOTH ALG AND MANEUVERING FLIGHT. IN FREE FLIGHT, MUCH OF THE REQUIRED PITCH CONTROL ACTIVITY CONSISTS OF SMALL DEFLECTIONS AROUND THE STRONG CENTERING SPRING DETENT. THE PILOT IS DEPRIVED OF TRUE ANTICIPATORY FEEL FOR AIRPLANE RESPONSE TO THESE SMALL INPUTS BY THE ANTIALLEE BREAKOUT FORCES. THIS IS A PROBLEM PREVIOUSLY ENCOUNTERED IN RESEARCH SIMULATORS. IT DOES NOT SERIOUSLY AFFECT AIRPLANE CONTROL WITH POSSIBLE EXCEPTION OF LOW TAKEOFF, BUT IT CAUSES HIGHER PILOT WORKLOAD IN ITERATING SMALL PITCH INPUTS AND IS IRRITATING.



\*\*\*\*\* ZEROS INDICATE NO RATING BY PILOT \*\*\*\*\*

# SAILPLANE 5 DATA

TASK

## DESCRIPTION OF TASKS

1

2

PILOT  
3

4

5

6

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AVER. STD DEV

- C. PILOT OPIN OF LONG. HANDLING
1. EASE OF EST & MAIN CON AIRSPEED
2. PLANE TRIM SYS OVER SPEED RANGE
3. PITCH SENSITIVITY
4. STICK FORCE GRADIENT
5. STICK FORCE STABILITY
6. STICK FREE STABILITY
7. RETURN TO TRIM
8. MANEUVERING RESPONSE
9. PHUGOID CHARACTERISTICS
10. DIVE RECOVERY

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7B AVER. AND STD. DEV. OF SUBTASKS(EX 1+2+...)

4.5 3.7 3.4 2.0 2.4 .5 .0 .7 .0 .0 3.0 .9 3.7 1.3 3.4 2.14

TASK

PILOT

## COMMENTS

PITCH RESPONSE TO CONTROL INPUTS IS LIKE ACCELERATION COMMAND - CHECKING MOTION FOLLOWS MOST STICK INPUTS - OVERSHOOT TENDENCY UNABLE TO TRIM TO FULL SPEED. TRIM CAPABILITY STOPS AT ABOUT 75% PDKT TOO SENSITIVE BUT NOT AS BAD AS SAILPLANE 3

EXTREMELY LIGHT

DIVERGES TOO EXTREME

POSITIVE STICK FORCES REQUIRED TO CHANGE SPEED.

EXTREMELY LIGHT GRADIENT

DIVERGES TOO EXTREME

NO RESPONSE TO STEP ELEVATOR INPUT IS APPRECIABLY DELAYED, MAKING LIGHT PITCH STEERING DIFFICULT.

FRICTION BAND TOO WIDE TO RETURN EXACTLY.

TRIM PDKT LOW 85 HIGH 60 WITH VTRIM 60KT. AFT STICK FORCE AT 67KT IS SEVERAL OUNCES. FWD STICK FORCE AT 60KTS IS ABOUT 2.25.

IN COMBINATION WITH REVERSED STICK FORCES MAKES FOR POOR MANEUVERING CHARACTERISTICS

EXCELLENT

DIVERGES TOO EXTREME

QUICKLY DIVERGES AT HIGH SPEED.

HEAVILY DIVERGENT

VTRIM 10KT; STRONGLY DIVERGENT-DID NOT LET IT COMPLETE A FULL CYCLE

NO PROBLEMS FOUND

DIVE RECOVERY NEGATIVE FORWEIGHT

RECOVERING FROM DIVE (100-120KTS) AFTER WINOVER IS VERY UNPLEASANT. THE STICK MUST BE HELD FIRMLY TO RESTRAIN IT. ALTERATIONS IN TRAJECTORY MUST BE MADE BY POSITIVELY DISPLACING THE STICK IN ESTIMATED AMOUNT AND HOLDING IT RIGID. THIS SHIP CANNOT BE FLOWN BY PRESSURE OR FEEL-ONLY BY STICK POSITION.

AT 60KTS QUICKLY DIVERGENT PHUGOID OSCILLATIONS; SOMEWHAT BETTER DAMPING A LITTLE FLOW ON PRECISE ATTITUDE CHANGES. NO UNPLEASANT SURPRISE WITH FLAP SETTING.

TRIM WITH SCHED DOWN KNOW UNCOMFORTABLE AND AWKWARD TO OPERATE

PHUGOID STRONGLY DIVERGENT-FRICTION VERY LOW IN SYSTEM (6000)

\*\*\*\*\* ZEROS INDICATE NO RATING BY PILOT \*\*\*\*\*

# SAILPLANE 6 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV							
81	C. PILOT OPIN OF LONG. HANDLING	.00	.00	.00	.70	.00	.00	.00	.667	.063							
82	1. RISE OF EST & MAIN CON AT SPEED	.00	1.00	.00	.70	.00	.00	.00	.577	.000							
83	2. PLANE TRIM SYS OVER SPEED RANGE	.00	.00	.00	.70	.00	.00	.00	.600	1.020							
84	3. PITCH SENSITIVITY	.00	.00	.00	.70	.00	.00	.00	.667	.491							
85	4. STICK FORCE GRADIENT	.00	.00	.00	.70	.00	.00	.00	.533	1.247							
86	5. STICK FIXED STABILITY	.00	.00	.00	.70	.00	.00	.00	.000	.839							
87	6. STICK FREE STABILITY	.00	.00	.00	.70	.00	.00	.00	.200	.800							
88	7. RETURN TO TRIM	.00	.00	.00	.70	.00	.00	.00	.000	.768							
89	8. MANEUVERING RESERVE	.00	2.00	.00	.70	.00	.00	.00	.577	.000							
90	9. PHANOID CHARACTERISTICS	.00	.00	.00	.70	.00	.00	.00	.000	.000							
91	10. DIVE RECOVERY	.00	2.00	.00	.70	.00	.00	.00	.000	.000							
70	AVER. AND STD. DEV. OF SUBTASKS(EX 1-2-...)	.0	.0	1.4	.5	2.4	.8	2.0	.4	2.0	.5	2.7	.8	1.7	.4	2.1	.73

TASK	PILOT	COMMENTS
81		VERY EASY WITHIN TRIM RANGE. STICK FORCES ARE ON HEAVY SIDE.
82		POWERFUL AND POSITIVE
83		RAN OUT OF TRIM AROUND 74IAS
84		HIGH TRIM SPEED 75IAS
85		NO TRIM BEYOND 78
86		GOOD
87		HIGH, BUT GOOD FOR TRAINER
88		POSITIVE
89		POSITIVE
90		FOR AIRSPEED TOO POWERFUL
91		HIGH, BUT GOOD FOR TRAINER
92		WATER TO BE POSITIVE
93		POSITIVE
94		POSITIVE
95		EXCESSIVE, HEAVY FORCES ARE REQUIRED TO CHANGE AIRSPEED
96		POSITIVE
97		POSITIVE
98		FOR TRIM 6000
99		GOOD FREE RETURN
100		1-2-3 EYES
101		TOO STRONG A TENDENCY
102		VTRIM 52IAS LOW 58 HIGH 54; VTRIM 65IAS LOW 58 HIGH 79
103		GOOD POSITIVE
104		POSITIVE
105		POSITIVE STICK FORCE/ICE
106		WINDY DAMPED
107		UNSTABLE PHANOID AT 60KTS
108		NEUTRAL
109		VTRIM 52IAS 22SEC PERIOD; VTRIM 65IAS 26 SEC PERIOD
110		GOOD - A LITTLE LIGHT FOR TRAINER
111		NO UNDERSHOCK CHARACTERISTICS WERE NOTED
112		SHORT PERIOD HEAVILY DAMPED
113		STICK GRADIENTS ARE LITTLE TOO HEAVY. SOME BUFFETING WELL INTO
114		CRUISING SPEED RANGE. RAN OUT OF TRIM AROUND 76KTS. SOFTNESS IN
115		STEADY ATTITUDE CHANGES
116		EXCELLENT CONTROL CHARACTERISTICS FOR TRAINING MISSION

\*\*\*\*\* ZEROS INDICATE NO RATING BY PILOT \*\*\*\*\*

# SAILPLANE 1 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3			4	5	6	7	AVER.	STD DEV				
D. PILOT OPINION OF LATERAL HANDLING	1. AILERON FORCE GRADIENT	1.00	1.00	1.00			.00	.00	.00	.00	1.000	.000				
	2. ROLLER FORCE GRADIENT	.00	.00	.00			.00	.00	.00	.00	1.000	.000				
	3. ROLL RATE OVER SPEED RANGE	.00	.00	.00			.00	.00	.00	.00	1.000	.000				
	4. SIDESLIP CHARACTERISTICS	.00	.00	.00			.00	.00	.00	.00	1.000	.000				
	5. EASE OF TURN ENTRY	.00	.00	.00			.00	.00	.00	.00	1.000	.000				
	6. YAW DUE TO AILERON	.00	.00	.00			.00	.00	.00	.00	1.000	.000				
	7. YAW DUE TO ROLL	.00	.00	.00			.00	.00	.00	.00	1.000	.000				
	8. EASE OF RAIN. 0.785RAD BANK TURN	.00	.00	.00			.00	.00	.00	.00	1.000	.000				
	9. EASE OF RAIN. 1.047RAD BANK TURN	.00	.00	.00			.00	.00	.00	.00	1.000	.000				
	79 AVER. AND STD. DEV. OF SUBTASKS (EX 1,2,...)	1.3	.5	1.2	.6	1.0	.5	1.7	.7	2.2	.4	1.9	.8	2.0	.8	1.7

TASK	PILOT	COMMENTS
32	1	VERY PLEASANT
33	1	CONTROL HARMONY VERY GOOD
34	1	OCCASIONALLY TOO LIGHT
35	1	EXCELLENT
36	1	ABOUT .250 TO .262 RAD./SEC AT SPEEDS CHECKED
37	1	.262 RAD/SEC AT 32 KIAS, .262 RAD/SEC AT 37 KIAS
38	1	AILERON FORCE REVERSED BUT GOOD OTHERWISE
39	1	ABOUT .262 RAD BANK REQ FOR MAX RUDDER DEFLECTION FOR CONSTANT HEAD
40	1	POSITIVE STABILITY HOWEVER A/S BLANKS OUT WITH YAW
41	1	RUDDER LOCKS
42	1	STEADY HEADING SIDESLIP—RUDDER FORCE GRADIENT LIGHTENS AFTER ABOUT
43	1	1/2 THROW, BUT NO REVERSE—FULL RUDDER REQUIRES .262 RAD BANK—SLIGHT
44	1	PITCH UP—LIGHTLY POSITIVE DIBEDRAL EFFECT
45	1	VERY EASY
46	1	VERY LITTLE RUDDER REQUIRED FOR INITIAL ROLL, SLIGHTLY MORE FOR LATER
47	1	VERY NOTICEABLE, BUT STILL IT IS POSSIBLE TO MAKE A GOOD TURN WITH
48	1	AILERONS ONLY
49	1	VERY EASY TO MAINTAIN COORDINATED CONTROL
50	1	ABOUT .262 RAD RUDDER PITCH
51	1	FOR PITCH UP ON WING WITH RUDDER—.262 RAD ROLL IN 5 SEC WITH FULL
52	1	RUDDER AT 32 KIAS
53	1	ONE OF THE BEST
54	1	GOOD—SLIGHT AMOUNT OF TOP STICK REQUIRED
55	1	EXCELLENT
56	1	EASE AS 0.8
57	1	VERY LIGHT AND RESPONSIVE
58	1	SUPERB COORDINATION IN MANEUVERING FLIGHT
59	1	EXCELLENT FOR THERMALING
60	1	SPIRAL STABILITY NEUTRAL—VERY GOOD—PITCH ROLL CONTROL AND RESPONSE
61	1	HARMONY IS VERY GOOD

\*\*\*\*\* ZEROS INDICATE NO RATING BY PILOT \*\*\*\*\*

# SAILPLANE 2 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVR.	STD DEV							
32	D. PILOT OPINION OF LATERAL HANDLING	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.000	.700							
33	1. AILERON FORCE GRADIENT	1.1+000	2.00	2.00	2.70	2.00	3.00	2.00	1.43	.250							
34	2. RUDDER FORCE GRADIENT	1.1+000	2.00	2.00	2.70	2.00	3.00	2.00	1.43	.250							
35	3. ROLL RATE OVER SPEED RANGE	2.00	2.00	2.00	2.70	2.00	3.00	2.00	1.43	.250							
36	4. STOEGLIP CHARACTERISTICS	3.00	2.00	2.00	2.70	2.00	3.00	2.00	1.43	.250							
37	5. EASE OF TURN ENTRY	2.00	2.00	2.00	2.70	2.00	3.00	2.00	1.43	.250							
38	6. YAW DUE TO AILERON	1.00	2.00	2.00	2.70	2.00	3.00	2.00	1.43	.250							
39	7. YAW DUE TO ROLL	3.00	2.00	2.00	2.70	2.00	3.00	2.00	1.43	.250							
40	8. EASE OF MAIN. 0.788RAD BANK TURN	2.00	2.00	2.00	2.70	2.00	3.00	2.00	1.43	.250							
41	9. EASE OF MAIN. 1.047RAD BANK TURN	2.00	2.00	2.00	2.70	2.00	3.00	2.00	1.43	.250							
79	AVR. AND STD. DEV. OF SUBTASKS(EX 1,2,...)	1.9	.7	2.1	.3	2.1	.6	2.5	.9	2.8	.6	2.1	.8	3.0	.8	2.4	.80

TASK	PILOT	COMMENTS
32	3	EXCESSIVE FRICTION CONTROL HARD NOT GOOD--FOR LONG PERIODS OF TURNING FLT. IT BECAME OBVIOUS THAT AILERON FORCES ARE TOO HEAVY. JUST ABOUT RIGHT FOR PURE ROLL VERY PLEASANT RUDDER NOT EFFECTIVE ENOUGH AT LOW SPEEDS WHEN EXECUTING RAPIDLY APPROX 3.5 SEC AT TURNING SPEEDS ABOUT 30RAD/SEC AVERAGE VTRIM 52IAS .48RAD/SEC; VTRIM 52IAS .38RAD/SEC NOT CHECKED SPEED DOES NOT PROBLEM. RUDDER FORCE REVERSES ONLY LITTLE BANK REQUIRED FOR MAXIMUM RUDDER DEFLECTION FOR CONSTANT HEADING FLT. RUDDER OVERBALANCES BUT NO PROBLEM. VTRIM 52 OF 21" SPIRAL STABILITY SLIGHTLY NEGATIVE. MODERATE PITCH--UNUSUAL RUDDER OVER BALANCE ABOUT 1/2 DEFLECTION RUDDER INSUFFICIENT BUT EVEN SO, THE TURN ENTRY WAS GOOD NOT TOO EASY HAVE TO WORK AT RUDDER TO COORDINATE AVERAGE REVERSE YAW VERY DIFFICULT TO KEEP YAW STRING CENTERED RUDDER KEEP WORKING TO CENTER OF YAW STRING CAN BE FLOWN HANDS OFF FAIRLY DIFFICULT AT LOWER SPEEDS NO ELEVATOR FORCE WORK TO COORDINATE TENDS TO WING WALK FAIRLY DIFFICULT AT LOWER SPEEDS NO ELEVATOR FORCE WORK TO COORDINATE 3 BEAK AT LOW SPEED 14SEC 43-SPAS 16000 AT HIGH SPEED 14SEC AT 70-871 4.5-7 WOULD BE BETTER WITH MORE EFFECTIVE RUDDER LATERAL-DIRECTIONAL HANDLING IS FAIRLY POOR. DIFFICULT TO MAINTAIN TURN COORDINATION. AT LOWER SPEEDS THERE MUST BE SOME SEPARATION ON THE ELEVATOR. RESULTING NIBBLE FEEDS BACK TO PILOT VIA PITCH STICK. ROLLING OSCILLATION IS ALSO ENCOUNTERED DURING LOW SPEED SPIRALING. LEARNING CURVE FOR TURN COORDINATION IS FAIRLY GRADUAL ON SAILPLANE 2. RUDDER DEFLECTION IS ACCOMPANIED BY CHANGED CHARACTERISTICS STOEGLIP--LATERAL POSITIVE. HOWEVER, EXPERIENCED RUDDER LOCK BOTH DIRECTIONS. ALSO LOSE A/Z WITH ABOUT 1/2 RUDDER DEFLECTION. GIVES GOOD CONFIDENCE FOR SMALL THERMAL TURNING. NOT ENOUGH RUDDER TO COORDINATE INITIAL MODERATE RATE TURN ENTRY. STRONG PITCHUP WITH STOEGLIP VERY UNDESIRABLE

\*\*\*\*\* ZEROS INDICATE NO RATING BY PILOT \*\*\*\*\*

# SAILPLANE 3 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV
	D. PILOT OPINION OF LATERAL HANDLING	1.50	2.00	2.50	2.00	2.00	2.00	2.00	2.200	.510
	1. AILERON FORCE GRADIENT	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.857	.748
	2. RUDDER FORCE GRADIENT	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.857	.748
	3. ROLL RATE OVER SPEED RANGE	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.857	.748
	4. SIDESLIP CHARACTERISTICS	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.857	.748
	5. EASE OF TURN ENTRY	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.857	.748
	6. YAW DUE TO AILERON	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.857	.748
	7. YAW DUE TO ROLL	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.857	.748
	8. EASE OF MAIN. 0.785RAD BANK TURN	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.857	.748
	9. EASE OF MAIN. 1.047RAD BANK TURN	1.00	1.00	1.00	1.00	1.00	1.00	1.00	.857	.748
79	AVER. AND STD. DEV. OF SUBTASKS(EX 1,2,..)	1.3	.5 2.1	.6 2.0	.4 1.4	.7 2.4	.6 2.0	.7 2.8	.6 2.1	.81

TASK	PILOT	COMMENTS
		FLEXIBLE WING ON SAILPLANE 5 MAKES IT WORSE LIGHT, MAYBE TOO MUCH SO. AILERON-ELEVATOR FORCE HARMONY-EXCELLENT PLEASANT TOOK ATTENTION EFFORT TO COORDINATE OVERBALANCES AT 3/4 DEFLECTION NO VARIATION OBSERVED; ADEQUATE THROUGHOUT. ABOUT .349RAD/SEC AT SPEEDS CHECKED VTHIN 48KTS .384RAD/SEC; 80KTS .524RAD/SEC RUDDER WEAR. PITCHES NOSE DOWN MODERATELY PLEASANT, ALTHOUGH FORCE REVERSAL OCCURS. RUDDER RETURNS TO NEUTRAL WHEN WINGS ARE LEVELED. POSITIVE AT 60 YAS; FULL RUDDER DEFLECTION WILL RESULT IN RUDDER LOCK! ALSO A LOSS OF AIRSPEED. RUDDER FORCE LIGHTENED BUT NEVER ZERO OR REVERSED. BUFFET/OVERBALANCE IN RUDDER IN BOTH DIRECTIONS, PITCH DOWN WITH S/LIP LESS RUDDER REQUIRED THAN SAILPLANE 2 AVERAGE ADVERSE YAW TAKES ATTENTION TO RUDDER SEEMS PRONOUNCED. HAVE TO MODULATE RUDDER TO COORDINATE. NO PROBLEM RUDDER NO PROBLEM RUDDER AND STICK; SMALL GRADIENT 0 STICK FORCE/SEC PLEASANT IN TURNS. ABOVE 26 TURNS WILL SELF TIGHTEN. TAIL BUFFET WITH AIR BRAKE OPEN SIDESLIPS ARE NOT OBJECTIONABLE PLEASANT LATERAL HANDLING, BUT FALLS SHORT OF SAILPLANE 1 OR 5. ROLL COORDINATION NO PROBLEM-AILERONS VERY EFFECTIVE BELOW STALL SPD 130

\*\*\*\*\* ZEROS INDICATE NO RATING BY PILOT \*\*\*\*\*

# SAILPLANE 4 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV							
33	D. PILOT OPINION OF LATERAL HANDLING	.00	N.00	N.00	N.00	N.00	N.00	N.00	N.200	.800							
34	1. AILERON FORCE GRADIENT	.00	N.00	N.00	N.00	N.00	N.00	N.00	N.167	.373							
35	2. RUDDER FORCE GRADIENT	.00	N.00	N.00	N.00	N.00	N.00	N.00	N.167	.373							
36	3. ROLL RATE OVER SPEED RANGE	.00	N.00	N.00	N.00	N.00	N.00	N.00	N.167	.373							
37	4. SIDESLIP CHARACTERISTICS	.00	N.00	N.00	N.00	N.00	N.00	N.00	N.167	.373							
38	5. EASE OF TURN ENTRY	.00	N.00	N.00	1.00	N.00	N.00	N.00	N.000	.577							
39	6. YAW DUE TO AILERON	.00	N.00	N.00	N.00	N.00	N.00	N.00	N.000	.800							
40	7. YAW DUE TO ROLL	.00	N.00	N.00	1.00	N.00	N.00	N.00	N.200	.800							
41	8. EASE OF MAIN. 0.785RAD BANK TURN	.00	N.00	N.00	1.00	N.00	N.00	N.00	N.200	1.000							
	9. EASE OF MAIN. 1.047RAD BANK TURN	.00	N.00	N.00	1.00	1.00	N.00	N.00	N.200	1.000							
79	AVER. AND STD. DEV. OF SUBTASKS(EX 1,2,...)	.0	.0	1.9	.3	2.1	.2	1.5	.7	2.2	.0	2.2	.4	3.1	.6	2.2	.76

TASK	PILOT	COMMENTS
33	3	PLEASANT
34	3	PLEASANT
35	3	ABOUT 3.5 SEC
36	3	CLOSER WITH FLAPS DOWN
37	3	ROLL RATE IS ADEQUATE BUT NOT AS GOOD AS THE OTHER HIGH PERFORMANCE
38	3	SAILPLANES
39	3	ABOUT .25RAD/SEC
40	3	4 SEC AT 0 FLAP 30IAS, 5SEC AT .209RAD FLAP AT 30IAS.
41	3	VTRIM 30IAS .105RAD FLAP .38RAD/SEC.
42	3	SEEMED TO TUCKER IN PITCH IN RIGHT FWD SLIP
43	3	PITCH DOWN
44	3	SUFFICIENT RUDDER TO BALANCE AILERON CONTROL
45	3	WING ROCKS AT 81 FEET ONSET. GOOD
46	3	BECAUSE OF STICK BACK PRESSURE WORKING AGAINST CENTERING SPRING
47	3	IN LAT-DIR MANEUVERS, SOME LATERAL MANEUVERS ARE HIGHLY OBJECTIONABLE
48	3	STRONGLY POSITIVE DIHEDRAL EFFECT. CONSIDERABLE TOP AILERON
49	3	REQD IN TURNS.

\*\*\*\*\* ZEROS INDICATE NO RATING BY PILOT \*\*\*\*\*

# SAILPLANE 5 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV
79	D. PILOT OPINION OF LATERAL HANDLING	2.00	3.00	2.00	.00	.00	4.00	2.00	2.600	.800
80	1. AILERON FORCE GRADIENT	.00	.00	.00	.00	.00	2.00	3.00	2.200	.400
81	2. RUDDER FORCE GRADIENT	.00	.00	.00	.00	.00	.00	4.00	2.600	.400
82	3. ROLL RATE OVER SPEED RANGE	.00	.00	.00	.00	.00	.00	4.00	2.300	1.077
83	4. SIDESLIP CHARACTERISTICS	.00	.00	.00	.00	.00	3.00	2.00	2.800	.748
84	5. EASE OF TURN ENTRY	.00	.00	.00	.00	.00	4.00	3.00	3.500	1.020
85	6. YAW DUE TO AILERON	.00	.00	.00	.00	.00	4.00	3.00	3.500	1.549
86	7. YAW DUE TO ROLL	1.00	1.00	1.00	.00	.00	2.00	1.00	1.200	.000
87	8. EASE OF MAIN. 0.785RAD BANK TURN	1.00	1.00	1.00	.00	.00	2.00	1.00	1.200	.400
88	9. EASE OF MAIN. 1.047RAD BANK TURN	2.00	1.00	1.00	.00	.00	2.00	2.00	1.500	.440
79	AVER. AND STD. DEV. OF SUBTASKS(EX 1,2,..)	1.9	.3	2.2	.9	1.9	.9	.0	.0	.0
									3.4	1.4
									2.6	.9
									2.4	
										1.06

TASK	PILOT	COMMENTS
79		PLEASANT, FAIRLY LARGE TOP AILERON REQUIRED.
80		LITTLE TOO HIGH OUTSIDE THE DEADBAND.
81		TOO HEAVY (NOT ENOUGH MECHANICAL ADVANTAGE)
82		SEC AT 50KTS 1.09RAD FLAP, 4 SEC AT 60KTS 0 FLAP
83		SLOW BUT SURPRISINGLY GOOD.
84		LOW VTRIM 60KT FLAP 0 262RAD/SEC
85		HEAVY, STABLE AILERON FORCES AND DISPLACEMENTS IN SIDESLIP. RUDDER
86		LOCKS-ABOUT 178N PEDAL FORCE REQD TO UNLOCK AT 70KTS. VERY LARGE
87		SIDESLIP ANGLES POSSIBLE. CONTROL OK.
88		RUDDER OVERBALANCE AT 3/4 DEFLECTION.
89		LARGE AILERON AND RUDDER INPUTS REQD.
90		RUDDER SUFFICIENT TO BALANCE
91		ABOUT THE SAME AS SAILPLANE 3
92		CAN BE BALANCED WITH RUDDER AT THERMALING SPEEDS.
93		EXCELLENT
94		EXCELLENT
95		IF SIZE AND SPAN OF SHIP WERE TAKEN INTO CONSIDERATION THE 2 RATINGS
96		WOULD BE BETTER
97		SURPRISINGLY GOOD LATERALLY FOR ITS SIZE.
98		IN SIDESLIP WITH FULL RUDDER, GLIDER FLIES ALMOST SIDEWAYS. PEDAL
99		FORCE REVERSES DIRECTION. STILL GOOD CONTROL IS MAINTAINED AND LFSS
00		BUFFETING IS EXPERIENCED THAN IN MOST OTHER SHIPS. FAIRLY WIDE
01		DEADBAND ON ACTION OF RUDDER PEDAL OBSERVED. SUDDEN REMOVAL OF
02		RUDDER DEFLECTION EXCITED A WELL-DAMPED OSCILLATION OF THE FUSELAGE
03		WHEN FLYING IN SMOOTH AIR.
04		VERY STABLE IN TURN, VERY LITTLE TOP AILERON REQUIRED

\*\*\*\*\* ZEROS INDICATE NO RATING BY PILOT \*\*\*\*\*

# SAILPLANE 6 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV							
30	D. PILOT OPINION OF LATERAL HANDLING	.00	.00	.00	.00	.00	.00	.00	.000	.000							
31	1. AILERON FORCE GRADIENT	.00	.00	.00	.00	.00	.00	.00	.000	.000							
32	2. RUDDER FORCE GRADIENT	.00	.00	.00	.00	.00	.00	.00	.167	.073							
33	3. ROLL RATE OVER SPEED RANGE	.00	.00	.00	.00	.00	.00	.00	.500	.766							
34	4. SIDESLIP CHARACTERISTICS	.00	.00	.00	.00	.00	.00	.00	.600	.490							
35	5. EASE OF TURN ENTRY	.00	.00	.00	.00	.00	.00	.00	.900	.788							
36	6. YAW DUE TO AILERON	.00	.00	.00	.00	.00	.00	.00	.900	.500							
37	7. YAW DUE TO ROLL	.00	.00	.00	.00	.00	.00	.00	.450	.500							
38	8. EASE OF MAIN. 0.785RAD BANK TURN	.00	.00	.00	.00	.00	.00	.00	.950	.500							
39	9. EASE OF MAIN. 1.047RAD BANK TURN	.00	.00	.00	.00	.00	.00	.00	.950	.500							
79	AVER. AND STD. DEV. OF SUBTASKS(EX 1,2,...)	.0	.0	2.4	.5	1.9	.6	2.4	.5	2.6	.4	3.2	1.2	2.1	.6	2.4	.81

TASK	PILOT	COMMENTS
33	3	FEELS BETTER THAN PITCH STICK GRADIENT
34	3	GOOD
35	3	TOO HEAVY
36	3	GOOD
37	3	HIGH RUDDER FORCE TO COORDINATE
38	3	VTRIM 52IAS .316RAD/SEC; VTRIM 78IAS .454RAD/SEC
39	3	SLIGHT PITCH/ROLL COUPLING-ALSO RUDDER A LITTLE WEAK
40	3	LOWER SINK RATE THAN OTHERS
41	3	LOUES BANK WITH FULL RUDDER FOR CONSTANT HEADING SLIP--NO RUDDER
42	3	LOCK. LOSE AIRSPEED AFTER APPROX. 1.26RAD YAW
43	3	SLIGHT PITCH DOWN WITH SIDESLIP. 1.75RAD BANK FOR FULL RUDDER, SLIGHT
44	3	DIRECTIONAL EFFECT AT 52IAS. NEUTRAL AT 78IAS
45	3	A LITTLE SLOW NEAR STALL.
46	3	VERY GOOD
47	3	ABOUT AVERAGE
48	3	VERY GOOD
49	3	BECAUSE OF HEAVY RUDDER FORCES, APPROX 89N IN MAINTAINING TURN
50	3	NEUTRAL LOW AMPLITUDE, LONG PERIOD
51	3	STICK FORCE/GE APPROX 9N
52	3	VERY GOOD
53	3	BOFFEYING
54	3	SAME AS .785RAD BANK
55	3	STICK FORCE/GE APPROX 22N
56	3	EXCELLENT EXCEPT NEAR STALL
57	3	EXCELLENT LATERAL-DIRECTIONAL CHARACTERISTICS MIXED SOMEWHAT BY
58	3	BUFFETING. GOOD ROLL RESPONSE
59	3	HARD TO COORDINATE RUDDER DUE TO UNHARMONIOUS FORCE (ONLY ABOUT 80N
60	3	BUT SEEMS HIGH RELATIVE TO STICK)
61	3	45 AND 60DEG- BANK LESS THAN EASY TO CONTROL, BUT STICK FORCE/GE
62	3	VERY LIGHT RESULTING IN OVERCONTROLLING ELEVATOR AND GETTING STALL.
63	3	BOFFEYING FREQUENTLY.
64	3	VERY GOOD- RUDDER COORDINATION REQD WOULD NOT BE ACCEPTABLE IN A
65	3	POWERED AIRPLANE, BUT AS SAILPLANES GO....



### SAILPLANE 1 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER. STD DEV	
42	E. PILOT OPIN OF PLANE STALLSPIN CHAR	1.50	.00	1.00	.20	.00	.00	.00	1.75 .78	
43	1. BUDDER,AILERON EFFECT DUR. STALL	.00	.00	.00	.20	.00	.00	.00	.535	
44	2. STALL WARNING	.00	.00	.00	.20	.00	.00	.00	.525	
45	3. AGGRAVATED STALL-TEND TO SPIN	1.00	.00	.00	.20	.00	.00	.00	1.000	
46	4. SUFFIC FORCE GRADIENT	.00	.00	.00	.20	.00	.00	.00	.728	
47	5. STALL RECOVERY, ALTITUDE LOSS	.00	.00	.00	.20	.00	.00	.00	1.000	
48	6. SPIN ENTRY	.00	.00	.00	.20	.00	.00	.00	.829	
49	7. SPIN RECOVERY	.00	.00	.00	.20	.00	.00	.00	.000	
50	8. STALL FROM TURN AT LOW SPEED	1.00	.00	.00	.20	.00	.00	.00	.500	
60	AVER. AND STD. DEV. OF SUBTASKS(EX 1:2...)	1.3	.5	2.1	1.1	1.4	.5	1.5	.7	.76

TASK	PILOT
1. Takeoff	1. Takeoff
2. Climb	2. Climb
3. Cruise	3. Cruise
4. Descent	4. Descent
5. Landing	5. Landing

**COMMENTS**

RUDDER EFFECTIVE, AILERONS INEFFECTIVE. RUDDER WILL NOT PICK UP  
BUT WILL ARREST FURTHER DROP  
ADULT  
BL-12T OCCURRED APPROX 1/2 KT ABOVE STALL  
THERE IS A DEFINITE TENDENCY TO FALL OFF TO ONE SIDE  
VERY SLOW WING DROP OFF, BUT EASILY RECOVERABLE BY RELEASING STICK  
EXCELLENT  
LOW  
VERY LITTLE  
PRESSURE LESS THAN 15M.  
MODERATE ENTRY RATE  
SLOW BUT PLenty OF TIME TO CATCH IT  
IMMEDIATE RECOVERY  
SLIGHTLY NEUTRAL ELEVATOR, SLIGHTLY OPPOSITE RUDDER  
NO AGGRAVATED STALL-SPIN ENTRY  
DIFFICULT TO DO  
STALL-SPIN CHARACTERISTICS ARE GOOD TO EXCELLENT. LACK OF SLIPPERI-  
NESS (ASSOCIATED WITH GLASS SHIPS) IS PROBABLY RESPONSIBLE FOR GOOD  
STALL CHARACTERISTICS  
ALL THE ABOVE GAVE GREAT CONFIDENCE IN SHIP TO WORK WEAK LIFT AT  
LOW ALTITUDE SAFELY  
LIGHT BUZZ AT 32IAS, STALL AT 32IAS(1[G]). TURNING STALL, CROSSED  
CONTROLS, AIRPLANE PRACTICALLY RECOVERS BY ITSELF! NOSE FALLS THRU  
AND AIRPLANE STARTS FLYING AGAIN. EXCELLENT CHARACTERISTICS-VERY SAFE

\*\*\*\*\* ZEROS INDICATE NO RATING BY PILOT \*\*\*\*\*

# SAILPLANE 2 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV							
43	E. PILOT OPIN OF PLANE STALLSPIN CHAR	1.00	1.00	1.00	1.00	1.00	1.00	1.00	2.200	1.600							
44	1. RUDDER; AILERON EFFECT DUR. STALL	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.857	1.125							
45	2. STALL WARNING	1.00	1.00	1.00	1.00	1.00	1.00	1.00	2.718	1.385							
46	3. AGGRAVATED STALL-TEND TO SPIN	1.00	1.00	1.00	1.00	1.00	1.00	1.00	2.143	1.726							
47	4. STICK FORCE GRADIENT	1.00	1.00	1.00	1.00	1.00	1.00	1.00	2.000	.756							
48	5. STALL RECOVERY; ALTITUDE LOSS	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.667	.745							
49	6. SPIN ENTRY	1.00	1.00	1.00	1.00	1.00	1.00	1.00	3.000	1.814							
50	7. SPIN RECOVERY	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.500	.500							
50	8. STALL FROM TURN AT LOW SPEED	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.857	1.125							
80	AVER. AND STD. DEV. OF SUBTASKS(EX 1,2,...)	1.0	.0	1.0	.0	2.2	.4	1.5	.4	2.5	.5	4.3	1.0	1.6	1.0	2.1	1.27

TASK	PILOT	COMMENTS
43	3	DURING STALLS RUDDER POOR, AILERON FAIRLY GOOD
44	3	ADEQUATE, SOME OF IT IS IN THE FORM OF CHANGING NOISE CHARACTER.
45	3	NO BUFFET WARNING-DIRECTIONAL STABILITY APPARENTLY DETERIORATES!
46	3	WANDERS IN YAW
47	3	NONE FOUND
48	3	ABOUT AVERAGE
49	3	15M
49	3	INCIDENT SPIN FAIRLY MILD
49	3	EASY RECOVERY
49	3	JUST RELAX AFT STICK FORCE
49	3	NO PROBLEM
50	3	PRIOR TO STALL THERE IS A TENDENCY OF ROLL OSCILLATIONS.
50	3	EASY STALL RECOVERY FROM EITHER TURN DIRECTION.
50	3	VERY SLIGHT PRE-STALL WARNING AND SUDDEN BREAK MAKE SHIP UNDESIRABLE
50	3	FOR EXTENSIVE THERMAL SOARING FOR A LONG TIME PILOT
50	3	VERY DOCILE STALLS; TURNING AND 1 G! STICK CAN BE HELD FULL AFT
50	3	NO AIRPLANE CAN BE REVERSED IN BANK--CAN BE FLOWN INDEFINITELY
50	3	IF HELD

\*\*\*\*\* ZEROS INDICATE NO RATING BY PILOT \*\*\*\*\*

# SAILPLANE 3 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV							
42	E. PILOT OPIN OF PLANE STALLSPIN CHAR	2.00	2.00	3.00	2.00	2.00	4.00	1.00	2.400	1.020							
43	1. RUDDER,AILERON EFFECT DUR. STALL	1.00	2.00	2.00	2.00	2.00	3.00	1.00	1.857	.639							
44	2. STALL WARNING	1.00	.00	.00	2.00	.00	3.00	.00	2.829	.904							
45	3. AGGRAVATED STALL-TEND TO SPIN	2.00	.00	.00	2.00	.00	4.00	.00	2.471	.604							
46	4. STICK FORCE GRADIENT	2.00	.00	.00	2.00	.00	4.00	.00	2.571	.728							
47	5. STALL RECOVERY, ALTITUDE LOSS	2.00	.00	.00	3.00	.00	3.00	.00	2.143	.639							
48	6. SPIN ENTRY	.00	.00	.00	2.00	.00	3.00	.00	2.333	.943							
49	7. SPIN RECOVERY	.00	.00	.00	2.00	.00	3.00	.00	2.000	1.000							
50	8. STALL FROM TURN AT LOW SPEED	2.00	1.00	2.00	2.00	2.00	2.00	1.00	1.667	.471							
80	AVER. AND STD. DEV. OF SUBTASKS(EX 1,2,..)	1.8	.7	1.8	.4	2.6	.5	2.4	.5	2.2	.4	3.1	.6	1.5	1.0	2.2	.83

TASK	PILOT	COMMENTS
42	1	3 KTS
43	1	ADEQUATE
44	1	VERY LIGHT AIRFRAME BUFFET APPROX. 2KTS ABOVE STALL.
45	1	LIGHT BUFFETING CLOSE (3KTS) TO STALL
46	1	NO WARNING
47	1	IT IS PRESENT IN THE GLIDER
48	1	WITH FULLY DEVELOPED STALL, A/C ROLLS OFF ON LEFT WING AND NOSE
49	1	DROPS APPROX. 5300' BELOW HORIZON
50	1	FALLS OFF ON WING AND ROTATES, EASY TO CONTROL
80	1	COULD BE IMPROVED--NOT ENOUGH FORCE
80	2	GOOD
80	2	NOT REALLY GOOD CUE FOR IMMINENT STALL
80	2	VERY LIGHT
80	2	IS MEYERS
80	2	LITTLE LOSS IN ALTITUDE
80	2	ALTITUDE LESS THAN 30M
80	2	15M /KTS STALL AT 42KTS
80	2	GONE QUITE RESISTANT
80	2	FAIRLY ABRUPT FALL-OFF TO ONE SIDE
80	2	NONE
80	2	SLOWER THAN OTHERS
80	2	VERY DOCLY
80	2	UNABLE TO STALL DUE TO LACK OF UP CONTROL TRAVEL
80	2	AILERON REMAINS EFFECTIVE THROUGHOUT STALL. FALLS OFF TO ONE SIDE
80	2	FAIRLY QUICKLY. DOES NOT RESPOND TO CORRECTIVE ACTION AS READILY
80	2	AS SAILPLANE 2
80	2	STALL CHARACTERISTICS EXCELLENT--AILERONS EFFECTIVE THROUGHOUT STALL-
80	2	PILOT HOLD STICK FULL AFT AND USE RUDDER AND AILERONS FOR CONTROL
80	2	FOR SOME TIME.

### SAILPLANE & DATA

TASK	PILOT	COMMENTS
0000	0000	GOOD
0001	0001	STALL WARNING OCCURS APPROX. 2 KTS ABOVE STALL.
0002	0002	NONE - LIGHT BUFFET AT STALL V STALL 30KTS FLAP 0
0003	0003	WING DROP UNCONTROLLABLE IF ABANDONED; BUT NOT ABANDON WING D/ OP
0004	0004	WING DROPS ABOVE STALL WITH FLAPS UP. OK WITH FLAPS.
0005	0005	SEEMED TO HAVE TENDENCY TO SPIN
0006	0006	DEFINITE FEELING OF BEGINNING AUTOROTATION
0007	0007	NO ADVERSE GRADIENT
0008	0008	IS METERS
0009	0009	NEGATIVE ALT LOSS
0010	0010	LESS THAN 15M
0011	0011	ABOUT 20M IN ICE STALL
0012	0012	IMMEDIATE WITH RELEASE OF BACK PRESSURE
0013	0013	UNABLE TO DO DUE TO LIMITED STICK TRAVEL.
0014	0014	ALT LOSS ABOUT 81 METERS.
0015	0015	GOOD
0016	0016	NO OBJECTIONABLE CHARACTERISTICS
0017	0017	WING DROP FOLLOWING ABUSED STALL IS UNCONTROLLABLE AND IS FOLLOWED
0018	0018	BY AUTOROTATIVE TENDENCY.

\*\*\*\*\* ZEROS INDICATE NO RATING BY PILOT \*\*\*\*\*

# SATPLANE 5 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV
42	E. PILOT OPIN OF PLANE STALLSPIN CHAR	2.00	2.00	2.00	.00	.00	2.00	1.00	2.00	.748
43	1. BUDDER, AILERON EFFECT DUR. STALL	2.00	2.00	2.00	.00	.00	2.00	1.00	2.00	.632
44	2. STALL WARNING	2.00	2.00	2.00	.00	.00	2.00	1.00	2.00	.985
45	3. AGGRAVATED STALL--TEND TO SPIN	2.00	2.00	2.00	.00	.00	2.00	1.00	2.00	.985
46	4. STICK FORCE GRADIENT	2.00	2.00	2.00	.00	.00	2.00	1.00	2.00	.690
47	5. STALL RECOVERY, ALTITUDE LOSS	2.00	2.00	2.00	.00	.00	2.00	1.00	2.00	.748
48	6. SPIN ENTRY	2.00	2.00	2.00	.00	.00	2.00	1.00	2.00	.707
49	7. SPIN RECOVERY	2.00	2.00	2.00	.00	.00	2.00	1.00	2.00	.500
50	8. STALL FROM TURN AT LOW SPEED	1.00	2.00	2.00	.00	.00	2.00	1.00	2.00	1.095
80	AVER. AND STD. DEV. OF SUBTASKS(EX 1+2+...)	1.7	.5 2.6	.9 2.0	.0	.0	.0	.0 2.6	.7 1.7 1.2 2.1	.85

TASK	PILOT	COMMENTS
42	7	OK UNTIL NEARLY FULL AFT STICK REACHED
43	7	BUFFET PROGRESSIVE WITH AFT STICK MOVEMENT
44	7	VERY POSITIVE
45	7	STALL SAKT LANDING FLAPS--VERY LIGHT BUFFET JUST BEFORE STALL
46	7	LARGE LONGITUDINAL STICK MOTIONS REQD NEAR STALL. AT STICK POSITION
47	7	WITHIN SCM OF APT STOP, SHIP WILL ENTER SPIN.
48	7	NONE
49	7	ADVISED STALL RESULTS IN EVENTUAL WING DROP BUT NO INCIPIENT SPIN
50	7	LIGHT
51	7	GOOD BUT NOT IN TURNS
52	7	12 METERS
53	7	SMALL
54	7	ABOUT 15M IF WING ALLOWED TO DROP
55	7	RELATIVELY RESISTANT
56	7	SLOW INCIPIENT SPIN QUICKLY STOPPED SINCE AILERON REMAINS EFFECTIVE
57	7	BEYOND THE STALL
58	7	OK WITH STICK RELEASED; NOT INSTANT RECOVERY, BUT FAIRLY PROMPT
59	7	NOT TRIED
60	7	CONSIDERABLE LOSS OF STICK FORCE GRADIENT UNDER 16G.
61	7	TENDS TO JUST PICK UP SPEED AND FLY OUT
62	7	NO TENDENCY TO FALL OFF TO EITHER SIDE AFTER STALL. STALL WARNING
63	7	IS IN THE FORM OF INCREASING TAIL SHAKE. OVERALL IMPRESSION OF
64	7	NICELY NO INCIPIENT SPIN. BETTER THAN MOST.
65	7	AILERON HAVE LAD BUT POSITIVE EFFECTIVENESS THROUGH STALL--EXCELLENT
66	7	STALL CHARACTERISTICS

\*\*\*\*\* ZEROS INDICATE NO RATING BY PILOT \*\*\*\*\*

# SAILPLANE 6 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV							
42	E. PILOT OPIN OF PLANE STALL SPIN CHAR	.00	.00	.00	.00	.00	.00	.00	4.333	1.247							
43	1. BUDDER, AILERON EFFECT DURING STALL	.00	.00	.00	.00	.00	.00	.00	4.000	.155							
44	2. STALL WARNING	.00	.00	.00	.00	.00	.00	.00	4.333	.247							
45	3. AGGRAVATED STALL-TEND TO SPIN	.00	.00	.00	.00	.00	.00	.00	4.000	.155							
46	4. STICK FORCE GRADIENT	.00	.00	.00	.00	.00	.00	.00	4.333	.247							
47	5. STALL RECOVERY, ALTITUDE LOSS	.00	.00	.00	.00	.00	.00	.00	3.667	.886							
48	6. SPIN ENTRY	.00	.00	.00	.00	.00	.00	.00	4.000	.118							
49	7. SPIN RECOVERY	.00	.00	.00	.00	.00	.00	.00	4.000	.000							
50	8. STALL FROM TURN AT LOW SPEED	.00	5.00	.00	2.00	2.00	9.00	4.00	4.000	2.517							
80	AVER. AND STD. DEV. OF SUBTASKS(EX 1:2:...) )	.0	.0	3.0	1.0	2.4	.5	2.5	.0	2.2	.4	5.0	1.6	2.0	1.3	3.3	1.75

TASK	PILOT	COMMENTS
43	7	WEAK JUST ABOVE STALL-INEFFECTIVE AFTER STALL
44	7	GOOD
45	7	STALL WARNING CONSISTED OF AIRFRAME PUFFET THAT BECAME APPARENT
46	7	SHORTLY ABOVE STALL. IF THERMALING IS CONDUCTED CONSTANTLY IN
47	7	STALL PUFFET THEN THE PILOT WILL IGNORE THE STALL PUFFET. NORMAL
48	7	STALL PUFFET SHOULD NOT OCCUR ABOVE THERMAL SPEED.
49	7	YES
50	7	TENDS TO ROLL LEFT AND NOSE PITCHES DOWN AT THE STALL.
80	7	RECOVERY IS GOOD.
80	7	LEFT WING DROPS, TENDENCY TO SPIN
80	7	SAILPLANE WANTS TO GO OVER THE TOP FROM A RIGHT TURN AND DIG IN
80	7	FURTHER TO THE LEFT FROM A LEFT TURN (FEET ON THE FLOOR, CROSS-
80	7	CONTROLLED STALLS)
80	7	GOOD
80	7	NOT MEASURED BUT CONSIDERABLE
80	7	LESS THAN 61M.
80	7	LESS THAN 61M.
80	7	AGGRAVATED STALL 61-91M.
80	7	MODERATE ENTRY RATE BUT POSITIVE ENTRY
80	7	FAIRLY QUICK
80	7	YES
80	7	ADEQUATE STALL WARNING, ABRUPT NOSE SLICE FOLLOWS SOME LATERAL
80	7	OSCILLATIONS JUST PRIOR TO STALL.
80	7	STICK FORCES DO NOT TELL YOU THAT YOU ARE ABOUT TO ENCOUNTER THE
80	7	MORE THAN 1.5 G. IT DOES SEEM TO INCREASE NEAR THE STALL AT 7 G.
80	7	HAS A TENDENCY TO YAW, ROTATE AND BURST THE NOSE FROM A CROSS-
80	7	CONTROLLED, ABUSED STALL

\*\*\*\*\* ZEROS INDICATE NO RATING BY PILOT \*\*\*\*\*

# SAILPLANE 1 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV						
51-57	F. PILOT OPIN. OF PLANE LANDING CHAR.	1.50	2.00	1.00	.00	.00	2.00	2.00	1.700	.400						
	1. PILOT VISIBILITY	.00	.00	.00	.00	.00	.00	.00	.571	.000						
	2. GLIDE SLOPE CONTROL	.00	.00	.00	.00	.00	.00	.00	.471	.728						
	3. STICK CONTROL: AIRB. EASE OF HOD.	.00	.00	.00	.00	.00	.00	.00	.143	.000						
	4. EASE OF LAND. AT INTENDED SPOT	.00	.00	.00	.00	.00	.00	.00	.471	.400						
	5. EASE OF CONTROL: SINK AT TOUCH.	.00	.00	.00	.00	.00	.00	.00	.500	.500						
	6. CONTROL DURING ROLLOUT	1.00	1.00	1.00	.00	2.00	2.00	2.00	1.429	.728						
61	AVER. AND STD. DEV. OF SUBTASKS(EX 1:2:..)	1.3	.5	1.1	1.3	.7	1.3	.7	2.0	.4	2.8	.7	2.0	.6	1.8	.86

TASK	PILOT	COMMENTS
51	1-2	VISIBILITY DOWN AND AFT RESTRICTED BY FUSELAGE AND WING SHORTS Y-TRIM--SLIGHT NOSE UP TRIM CHANGE WITH SPOILER DEPLOYMENT. MOMENTARY SKT DECAT STICK-FREE, THEN INCREASE TO ADD IT 4SKTS-VERY GO AIRBRAKES SUCK OPEN OUTSTANDING GROUND MANEUVERABILITY VERY EASY TO LAND AT WILL OVER THE NOSE VISIBILITY WEAK, SPOILERS COULD BE MORE POWERFUL. TAIL SKID RESTRICTS GROUND STEERING.

# SAILPLANE 2 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV							
51	F. PILOT OPIN. OF PLANE LANDING CHAR.	2.00	.00	2.00	.00	.00	5.00	2.00	2.750	1.200							
52	1. PILOT VISIBILITY	.00	.00	.00	.00	.00	.00	.00	1.429	.728							
53	2. GLIDE SLOPE CONTROL	.00	.00	.00	.00	.00	.00	.00	.000	.000							
54	3. STICK CONTROL: AIRB. EASE OF HOD.	.00	.00	.00	.00	.00	.00	.00	.143	.000							
55	4. EASE OF LAND. AT INTENDED SPOT	.00	.00	.00	.00	.00	.00	.00	.471	.728							
56	5. EASE OF CONTROL: SINK AT TOUCH.	.00	.00	.00	.00	.00	.00	.00	.286	.881							
57	6. CONTROL DURING ROLLOUT	.00	.00	.00	3.00	3.00	6.00	2.00	.471	.728							
61	AVER. AND STD. DEV. OF SUBTASKS(EX 1:2:..)	2.2	.9	2.0	.6	2.3	.5	2.7	.9	2.0	.4	4.2	.7	2.2	.7	2.5	1.01

TASK	PILOT	COMMENTS
51	1-2	GOOD AIRBRAKES A LITTLE WEAK COULD USE MORE EFFECTIVE DIVE BRAKES VERY LOW FORCE GRADIENT RESULTS IN OVERCONTROL. CONSTANT ATTITUDE CONTROL LOCK VERY POOR. UNLOCKING OF AIRBRAKES RESULTS IN DEPLOYMENT TO 1/2 OPEN IF UNRESTRAINED. A VERY POSITIVE FORCE IS REQUIRED TO CLOSE THE AIRBRAKES. I FEEL THAT YOU SHOULD BE ABLE TO SELECT AIRBRAKE RAPIDLY AND IT WILL REMAIN AT SELECTED POSITION WHEN THE CONTROL IS RELEASED. HAVE TO HOLD AGAINST FURTHER EXTENSION WHICH I PREFER TO HOLDING WITH GOOD AIRBRAKES COULD BE MORE EFFECTIVE LONGITUDINAL OR -DIRECT WIND EFFECT VERY GOOD VERY LOW FORCE GRADIENT AND SHORT CONTROL STICK RESULTED IN OVERC'TRI BETTER THAN SAILPLANE 1 INSUFFICIENT RODDER FOR ADEQUATE MANEUVERING. DIRECTIONAL TAKES A LITTLE EFFORT 2,3,4 INADEQUATE DIVE BRAKE EFFECTIVENESS. 6. SOME CONCENTRATION REQUIRED (LATERAL AND DIRECTIONAL) LANDING CHARACTERISTICS ARE BETTER THAN AVERAGE. NO TENDENCY TO GO TO EITHER SIDE. DIVE BRAKES WEAK. USE OF DRAG CHUTE NOT INCLUDED IN TEST EVALUATION. TOUCHDOWN CAN BE ACHIEVED BUT ONLY THRU USE OF EXCESSIVE SPEED.

\*\*\*\*\* ZEROS INDICATE NO RATING BY PILOT \*\*\*\*\*

# SAILPLANE 3 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV						
F. PILOT OPIN. OF PLANE LANDING CHAR.	1. PILOT VISIBILITY	2.000000	2.000000	2.000000	2.000000	2.000000	2.000000	2.000000	2.000000	2.000000						
	2. DIVE BRAKE CONTROL	2.000000	2.000000	2.000000	2.000000	2.000000	2.000000	2.000000	2.000000	2.000000						
	3. FLARE CONTROL FAIR. EASE OF MOD.	2.000000	2.000000	2.000000	2.000000	2.000000	2.000000	2.000000	2.000000	2.000000						
	4. RATE OF LAND. AT INTENDED SPOT	2.000000	2.000000	2.000000	2.000000	2.000000	2.000000	2.000000	2.000000	2.000000						
	5. EASE OF CONTROL. SINK AT TOUCH.	2.000000	2.000000	2.000000	2.000000	2.000000	2.000000	2.000000	2.000000	2.000000						
	6. CONTROL DURING ROLLOUT	2.000000	2.000000	2.000000	2.000000	2.000000	2.000000	2.000000	2.000000	2.000000						
	61 AVER. AND STD. DEV. OF SUBTASKS(EX 1:2:...)	2.7	.5	2.6	.4	2.5	1.7	2.5	1.7	3.4	2.7	2.8	.7	2.5	.4	2.7

TASK PILOT

## COMMENTS

EXCELLENT  
 AIR BRAKES A LITTLE WEAK  
 VERY LOW FORCE GRADIENT RESULTS IN SOME PORPOISING PRIOR TO FLARE.  
 LIGHT SUCK-OFF FORCES  
 VERY GOOD CONTROL BUT FAST  
 AIR BRAKE HAS A TENDENCY AFTER BEING UNLOCKED TO FLOAT TO APPROX.  
 3/4 EXTENDED POSITION. I FEEL THE AIR BRAKE SHOULD HAVE THE  
 CAPABILITY OF RAPID MOVEMENT BUT THE AIR BRAKE SHOULD REMAIN IN  
 THE SELECTED POSITION.  
 SLIGHT FALL DOWN WITH SPOILER EXTENSION AT 58 KTS.  
 NOT AS EASY AS SOME  
 AIR BRAKES COULD BE MORE EFFECTIVE  
 EASY TO CONTROL IN PITCH IN TURBULENCE  
 VERY LOW FORCE GRADIENT RESULTS IN SOME VERTICAL OSCILLATION DURING  
 THE FLARE  
 ROLLER FAIR--AILERONS FAIR  
 BRAKE CONTROL AHEAD TO APPLY WITHOUT TAKING HAND FROM CONTROL STICK  
 HOWEVER, FULL BRAKE APPLICATION RESULTED IN ONLY MINOR BRAKING ACTION  
 LOST CONTROL DURING ONE OF LANDINGS  
 MINOR BLOOPER AND TAILSKID FOR DIRECTIONAL CONTROL. A STEERABLE  
 TAIL WHEEL WOULD HELP.  
 2:3:4:5 COULD BE IMPROVED WITH MORE POWERFUL DIVE BRAKE  
 FAIR CROSSING CAPABILITY  
 FAIRLY EASY TO MAKE GOOD LANDING. TOUCHES DOWN AT HIGHER SPEEDS  
 THAN ONE WOULD LIKE TO.  
 LIMITED YAW CONTROL ON ROLLOUT.



\*\*\*\*\* ZFROS INDICATE NO RATING BY PILOT \*\*\*\*\*

# SAILPLANE & DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV							
01	F. PILOT OPIN. OF PLANE LANDING CHAR.	.00	.00	.00	.00	.00	.00	.00	.00	.00							
02	1. PILOT DISTURBANCE	.00	.00	.00	.00	.00	.00	.00	.00	.00							
03	2. OLIVE SLOPE CONTROL	.00	.00	.00	.00	.00	.00	.00	.00	.00							
04	3. ATTS. CONTROL. EASE OF MOD.	.00	.00	.00	.00	.00	.00	.00	.00	.00							
05	4. EASE OF LAND. AT INTENDED SPOT	.00	.00	.00	.00	.00	.00	.00	.00	.00							
06	5. EASE OF CONTROL. EASE AT TOUCH.	.00	.00	.00	.00	.00	.00	.00	.00	.00							
07	6. CONTROL DURING ROLLOUT	.00	.00	.00	.00	.00	.00	.00	.00	.00							
B1	AVER. AND STD. DEV. OF SUBTASKS(1-2...)	.0	.0	2.5	1.3	2.3	.4	2.5	1.3	3.3	1.1	2.7	.0	3.0	1.3	2.7	1.14

TASK	PILOT	COMMENTS
01	1	EXCELLENT
02	1	OR UNTIL FLARE THEN FLOATS IF SPEED IS TOO HIGH
03	1	EXCELLENT
04	1	SELECTION OF FLAPS FOR DRAG RESULTS IN LARGE PITCH ANGLES
05	1	HARD TO MODULATE FLAPS. HANDLE URGENTLY
06	1	NOT TRIED AT LOW SPEEDS. IT WOULD BE OBJECTIONABLE
07	1	AIN BRAKE (FLAPS) REQUIRE CONSTANT FORCE AND EFFORT TO SELECT AND
08	1	MAINTAIN DESIRED POSITION. BECAUSE OF HANDLE LOCATION AND TRAVEL
09	1	DIFFICULT TO OBTAIN MAX. FLAP TRAVEL. FORCES VERY HIGH AT MAX.
10	1	FLAP SPEED
11	1	FLAATED DURING FLARE
12	1	PRECISE SPEED CONTROL REQUIRED AT FLARE ENTRY POINT IF DROP-IN OR
13	1	LONG FLOAT ARE TO BE AVOIDED
14	1	INSUFFICIENT PRACTICE FOR OBJECTIVE EVALUATION OF THE FLAP SYSTEM
15	1	THE AIR BRAKE IS ON IN MOST SITUATIONS
16	1	THE AIR BRAKE IS VERY DIFFICULT TO MANIPULATE, I.E. TAKES
17	1	LARGE FORCE TO PUT IT WHERE I WANT TO MAINTAIN YES. IN ADDITION,
18	1	THE AIRPLANE ATTITUDE CHANGES DRASTICALLY TO WHERE I AM UNCERTAIN
19	1	OF FLIGHT PATH.
20	1	CHANGE OF TRIM FROM FLAPS -9 TO LANDING BRAKE CAUSES HIGH STICK
21	1	FORCES. FLAP CONTROL REQUIRES VERY HIGH FORCES TO UN-LOD AROUND
22	1	1500-1600RAD.
23	1	PHYSICALLY UNABLE TO SELECT 1-396RAD FLAPS IN FINAL STAGE OF APPROACH
24	1	HAVE TO HOLD HIGH FORCE ON FLAP HANDLE WITH LEFT HAND AND MAKE SMALL
25	1	PRECISE STICK INPUTS WITH RIGHT HAND TO EXECUTE 0 IDP PATH AND LOR.
26	1	ON THE FINAL LANDING. MADE A HIGH BASE LEG AND SELECTED LANDING
27	1	FLAPS. THEN CONTROLLED FLIGHT PATH WITH PITCH ATTITUDE ONLY. ACCEPTING
28	1	SPEED, WHICH BLEW OFF EARLY DURING FLARE. I CONSIDER THIS AN
29	1	UPWARD AND IMPRECISE METHOD. IT WOULD NOT OFFER THE PRECISION IN
30	1	FLIGHT PATH CONTROL WHICH IS AVAILABLE WITH THE METHOD OF CONTROLLING
31	1	AIR SPEED WITH MODULATION OF A DRAG DEVICE THROUGHOUT THE APPROACH.

\*\*\*\*\* ZEROS INDICATE NO RATING BY PILOT \*\*\*\*\*

# SAILPLANE 5 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV
51	F. PILOT OPIN. OF PLANE LANDING CHAR.	.50	.00	3.00	.75	.00	.00	3.00	2.00	.663
52	1. PILOT VISIBILITY	.00	.00	.00	.00	.00	.00	.00	1.00	.000
53	2. GIVE SLOPE CONTROL	.00	.00	.00	.00	.00	.00	.00	2.00	.000
54	3. AIRS. CONTROL+AIRS. EASE OF MOD.	.00	.00	.00	.00	.00	.00	.00	3.00	.000
55	4. EASE OF LAND. AT INTENDED SPOT	.00	.00	.00	.00	.00	.00	.00	3.00	.000
56	5. EASE OF CONTROL. SINK AT TOUCH.	.00	.00	.00	.00	.00	.00	.00	3.00	.000
57	6. CONTROL DURING ROLLOUT	.00	.00	.00	.00	.00	.00	.00	4.00	1.265
61	AVER. AND STD. DEV. OF SUBTASKS(1+2+...)	2.2	.4	2.7	.9	2.4	1.0	.0	.0	1.02

TASK	PILOT	COMMENTS
51		EXCELLENT COULD USE A LITTLE MORE AIR BRAKE EXCELLENT USE OF DRAG CHUTE NOT INCLUDED IN EVALUATION SLIGHT PITCH DOWN WITH SPEED BRAKE EXTENSION-500 GOOD EXCEPT SOME SUCK-OPEN FORCE ABOVE 65KTS. FAST BUT ROLLS FOR A LONG TIME FLEXIBLE WING FOOLS PILOT, MUST FLY SMOOTHLY LATERAL CONTROL VERY SLOW UNLESS FLAPS RAISED DURING ROLLOUT. RUMOR FAIR. CROSSWIND CAPABILITY LIMITED. DON'T LIKE TO PUT UP FLAPS DURING ROLLOUT. SO LATERAL CONTROL FORCES INCREASED--UNEVEN FORCE GRADIENT LONG ROLLOUT, COULD USE MORE BRAKING ACTION. CONTINUOUS PILOT ACTION NEED FOR STRAIGHT LINES LEVEL ROLLOUT. CROSSWIND CAPABILITY SEVERELY LIMITED, PROBABLY 15KT. VECTOR MAX. A STEERABLE TAIL WHEEL WOULD HELP MARGINAL YAW CONTROL ON GROUND FLAPS MUST BE RAISED AFTER TOUCHDOWN. THIS LANDING WAS CONDUCTED WITH WIND ABOUT 30TS STRAIGHT DOWN THE RUNWAY. MY RATING WOULD LIKELY BE WORSE(HIGHER) IN A CROSSWIND.

# SAILPLANE 6 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV
61	F. PILOT OPIN. OF PLANE LANDING CHAR.	.00	.00	2.00	.70	.00	2.00	3.00	2.553	.471
62	1. PILOT VISIBILITY	.00	.00	.00	.70	.00	.00	.00	1.00	.000
63	2. GIVE SLOPE CONTROL	.00	.00	.00	.70	.00	.00	.00	2.00	.000
64	3. AIRS. CONTROL+AIRS. EASE OF MOD.	.00	.00	.00	.70	.00	.00	.00	3.00	.000
65	4. EASE OF LAND. AT INTENDED SPOT	.00	.00	.00	.70	.00	.00	.00	3.00	.000
66	5. EASE OF CONTROL. SINK AT TOUCH.	.00	.00	.00	.70	.00	.00	.00	3.00	.000
67	6. CONTROL DURING ROLLOUT	.00	.00	.00	.70	1.00	.00	.00	1.553	.471
61	AVER. AND STD. DEV. OF SUBTASKS(1+2+...)	.0	.0	1.6	.4	1.7	.7	1.0	.0	.60

TASK	PILOT	COMMENTS
61		EXCELLENT GOOD--DUE TO DIVE BRAKE EFFECTIVENESS IT IS EASY TO MAKE DIFFICULT LANDING GOOD--POOR IF NOT GREASED WELL, VERY POOR EXCELLENT--BUT ONE HAS TO BE CAREFUL WITH BRAKES NEAR THE GROUND SLIGHT PITCH DOWN WITH SPOILER EXTENSION(GOOD CHARACTERISTIC) VERY GOOD EXCEPT AS VOTED VERY GOOD AIR BRAKES SUCK OPEN--MODERATE FORCE TO CLOSE. TENDENCY TO LAND HARD IF MORE THAN ABOUT 174 AIR BRAKE OPEN SHIP HAS VERY GOOD LANDING CHARACTERISTICS. LARGE SINK RATES REQUIRE DEFINITE PILOT ATTENTION VERY GOOD EXCEPT AIRPLANE IS NOT FORGIVING OF LETTING AIRSPEED DECAY BELOW 174S ON FINAL APPROACH

\*\*\*\*\* ZEROS INDICATE NO RATING BY PILOT \*\*\*\*\*

#### SAILPLANE 1 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV				
58	III. FLIGHT CHARACTERISTICS IN CONVECTION	1.00	1.00	1.00	.70	.00	1.00	.00	1.000	.000				
59	A. PILOT OPINION OF TOW	1.00	.00	1.00	.70	.70	2.00	1.00	1.500	.764				
60	1. EASE OF MAINTAINING POSITION	1.00	.00	1.00	.70	.00	1.00	.00	1.333	.745				
61	2. RESPONSE TO VERTICAL CURRENTS	1.00	.00	1.00	.70	.00	1.00	.00	1.333	.687				
62	3. RELEASE	1.00	.00	2.00	.70	2.00	2.00	.00	1.800	.400				
82	AVER. AND STD. DEV. OF SUBTASKS(EX 1:2+...)	1.0	.0	1.5	.5	1.3	.5	.0	2.7	.5	1.7	.5	1.6	.68

TASK	PILOT	COMMENTS
60	5	PITCH PRIMARILY--LAT/DIR-2
61	7	NO DIFFICULTY WAS EXPERIENCED DUE TO PRESENCE OF VERTICAL CURRENTS
62	7	HAD TO USE SLIGHT FORWARD STICK FORCE DURING TOW--TRIM NOT ADEQUATE
62	7	FORCE WAS VERY LOW HOWEVER

#### SAILPLANE 2 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV						
58	III. FLIGHT CHARACTERISTICS IN CONVECTION	1.50	.00	3.00	.00	1.50	3.00	3.00	2.500	.717						
59	A. PILOT OPINION OF TOW	1.50	.00	3.00	.70	1.50	3.00	3.00	2.417	.812						
60	1. EASE OF MAINTAINING POSITION	1.00	.00	3.00	.70	2.00	3.00	3.00	2.500	.957						
61	2. RESPONSE TO VERTICAL CURRENTS	1.00	.00	3.00	.70	2.00	3.00	3.00	2.500	.900						
62	3. RELEASE	1.00	.00	2.00	.00	.00	2.00	2.00	1.750	.433						
82	AVER. AND STD. DEV. OF SUBTASKS(EX 1:2+...)	1.3	.5	2.5	.5	2.7	.5	.0	2.5	.5	2.0	.0	3.0	.8	2.3	.77

TASK	PILOT	COMMENTS
60	5	GOT TO STAY WITH IT. DIRECTIONAL MOST OBVIOUS
61	3	GOT SOME TOW ROPE REBOUNDING
62	3	BELIEVE THAT THE BOUNCY RIDE IN TURBULENCE IS CAUSED BY WING FLEX
62	3	I WOULD RATE THE SAILPLANE ABOUT THE SAME HERE AS IN SMOOTH AIR.

#### SAILPLANE 3 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV						
58-62	III. FLIGHT CHARACTERISTICS IN CONVECTION	2.00	3.00	2.00	.00	.00	3.00	3.00	2.600	.400						
	A. PILOT OPINION OF TOW	1.50	3.00	2.00	.00	.00	3.00	3.00	2.517	.607						
	1. EASE OF MAINTAINING POSITION	1.00	3.00	2.00	.00	.00	3.00	3.00	2.500	.500						
	2. RESPONSE TO VERTICAL CURRENTS	1.00	4.00	2.00	.70	.00	3.00	3.00	2.333	.687						
	3. RELEASE	1.00	.00	3.00	.70	.00	2.00	2.00	2.000	.632						
82	AVER. AND STD. DEV. OF SUBTASKS(EX 1:2+...)	2.0	.0	3.5	.5	2.3	.5	.0	2.7	.5	2.0	.0	2.7	.5	2.5	.70

TASK	PILOT	COMMENTS
59	3	MODERATE CONTROL ACTIVITY REQD.
60	3	NO PROBLEMS
61	3	SOME TENDENCY OF NOSE TO PORPOISE.
62	3	TENDENCY TO PITCH WHEN ENCOUNTERING TURBULENCE
62	3	NO PROBLEMS
62	3	NOISY
62	3	SOME STICK INSTABILITY IN TURBULENCE
62	3	HIGH WORKLOAD IN RUDDERS AND AILERONS

\*\*\*\*\* ZEROS INDICATE NO RATING BY PILOT \*\*\*\*\*

#### SAILPLANE 4 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV
58	III. FLIGHT CHARACTERISTICS IN CONVECTION	.00	2.00	2.50	.00	.00	3.00	3.00	2.625	.415
59	A. PILOT OPINION OF TOW	.00	2.00	2.00	.00	.00	2.00	2.00	2.000	.000
60	1. EASE OF MAINTAINING POSITION	.00	2.00	2.00	.00	.00	2.00	2.00	2.000	.000
61	2. RESPONSE TO VERTICAL CURRENTS	.00	2.00	2.00	.00	.00	2.00	2.00	2.000	.000
62	3. RELEASE	.00	.00	3.00	.00	.00	2.00	2.00	2.333	.471
62	AVER. AND STD. DEV. OF SUBTASKS(EX 1+2+...)	.0	.0 2.0	.0 2.3	.5	.0 .0	.0 .0 2.0	.0 2.0 .0 2.1		.29

TASK	PILOT	COMMENTS
60	3	NO PROBLEM AT ALL
61	3	NOISY
62	3	GOOD
62	3	NO SIGNIFICANT DIFFERENCE FROM STILL AIR

#### SAILPLANE 5 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV
58	III. FLIGHT CHARACTERISTICS IN CONVECTION	2.00	5.00	2.00	.00	.00	4.00	3.00	3.200	1.166
59	A. PILOT OPINION OF TOW	1.50	5.00	.00	.00	.00	4.00	2.00	3.875	1.431
60	1. EASE OF MAINTAINING POSITION	2.00	2.00	.00	.00	.00	3.00	5.00	3.000	1.225
61	2. RESPONSE TO VERTICAL CURRENTS	2.00	2.00	.00	.00	.00	3.00	3.00	2.500	.500
62	3. RELEASE	1.00	.00	.00	.00	.00	3.00	2.00	2.000	.816
62	AVER. AND STD. DEV. OF SUBTASKS(EX 1+2+...)	1.7	.5 2.0	.0 .0	.0 .0	.0 .0 4.0	.0 3.3 1.2 2.5			.99

TASK	PILOT	COMMENTS
59	2	OK AT 70KTS, AT 80KTS WORSE THAN IN SMOOTH AIR. MUST FLY WITH STICK
59	2	RIGID.
62	2	CANNOT FLY PITCH BY PRESSURE, MUST FLY BY POSITION.
60	3	NO ROUGH AIR TOW NAGE
61	3	YAW AND ROLL RATES MAKE STAYING BEHIND TOWPLANE DIFFICULT IN ROUGH
62	3	THERMALS
62	7	LATERAL POSITIONING IS AN EASY TASK; PITCH IS DIFFICULT DUE TO OVERCONTROL TENDENCY

#### SAILPLANE 6 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV
58	III. FLIGHT CHARACTERISTICS IN CONVECTION	.00	3.00	2.00	.00	.00	5.00	3.00	3.000	1.225
59	A. PILOT OPINION OF TOW	.00	3.00	2.00	.00	.00	3.00	3.00	2.500	.433
60	1. EASE OF MAINTAINING POSITION	.00	2.00	2.00	.00	.00	3.00	3.00	2.000	.000
61	2. RESPONSE TO VERTICAL CURRENTS	.00	2.00	2.00	.00	.00	3.00	3.00	2.000	.000
62	3. RELEASE	.00	.00	2.00	.00	.00	2.00	2.00	2.000	.000
62	AVER. AND STD. DEV. OF SUBTASKS(EX 1+2+...)	.0	.0 2.0	.0 2.0	.0 .0	.0 .0 2.0	.0 2.0 .0 2.0			.00

TASK	PILOT	COMMENTS
61	3	NOT EXCESSIVE
62	3	SAME AS SMOOTH AIR
62	7	AIR SPEED FEELS OFF QUICKLY DURING PULLUP, REQUIRING PILOT ATTENTION
62	7	HIGHER WORKLOAD THAN IN SMOOTH AIR, OF COURSE, BUT NO UNUSUAL CHARACTERISTICS DUE TO TURBULENCE

\*\*\*\*\* ZEROS INDICATE NO RATING BY PILOT \*\*\*\*\*

# SAILPLANE 1 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV
63	B. PILOT OPINION OF CIRCLING FLIGHT	1.00	1.00	1.00	.00	.00	1.00	1.00	1.000	.000
64	1. LOWSPEED HANDLING	1.00	1.00	1.00	.00	.00	1.00	1.00	1.167	.373
65	2. STALL-SPIN SUSCEPTIBILITY	2.00	2.00	1.50	.00	.00	1.00	1.00	1.750	.382
66	3. EASE OF CENTERING THERMAL	1.00	1.00	2.00	.00	.00	1.00	1.00	1.533	.687
67	4. SPEED CONTROL	1.00	1.00	2.00	.00	.00	1.00	1.00	1.500	.500
63	AVER. AND STD. DEV. OF SUBTASKS(EX 1:2:..)	1.3	.4 1.3	.4 1.6	.4 .0	.0 2.2	.4 1.3	.4 1.7	.4 1.6	.56

TASK	PILOT	COMMENTS
63	2	BEST THERMAL MANEUVERING OF ANY SAILPLANE-PERHAPS DUE TO POWERFUL RUDDER
64	3	GOOD AILERON -- ROLL RESPONSE IN THERMALS; EASY TO MISLE GLIDER AROUND IN THERMALS
65	4	LAT-DYN QUALITIES EXCELLENT-VERY LOW WORKLOAD-LITTLE RUDDER REQ FOR TRIM COORDINATION-EXCELLENT CONTROL HARMONY, BOTH IN FORCES AND RESPONSES
66	7	
67	7	

# SAILPLANE 2 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV
63	B. PILOT OPINION OF CIRCLING FLIGHT	1.50	1.50	3.00	.00	.00	2.00	4.00	2.400	.970
64	1. LOWSPEED HANDLING	2.00	1.00	2.00	.00	.00	1.00	4.00	2.333	.898
65	2. STALL-SPIN SUSCEPTIBILITY	1.00	1.00	2.00	.00	.00	1.00	4.00	2.333	1.374
66	3. EASE OF CENTERING THERMAL	2.00	1.00	3.00	.00	.00	2.00	4.00	2.333	.745
67	4. SPEED CONTROL	1.00	1.00	4.00	.00	.00	1.00	3.00	2.167	1.213
63	AVER. AND STD. DEV. OF SUBTASKS(EX 1:2:..)	1.5	.5 1.3	.4 2.7	.4 .0	.0 3.2	.4 2.7	1.5 3.0	.7 2.4	1.11

TASK	PILOT	COMMENTS
64	3	HAS SOME UNDESIRABLE CHARACTERISTICS; RUFFETING, FEELS PRECARIOUS DUE TO STICK POSITION AFT WITH LOW FORCE AND YAW STRING OSCILLATION
65	4	AVERAGE
66	7	MORE DIFFICULT THAN OTHERS
67	7	FAIRLY DIFFICULT
63	7	1:3 RUDDER EFFECTIVENESS COULD BE IMPROVED. 4: WILL SPIRAL HANDS OFF FOR LONG PERIODS
64	7	LACK OF DIRECTIONAL STABILITY AND DIFFICULT TURN COORDINATION
65	7	LOW RUDDER EFFECTIVENESS
66	7	HIGH WORKLOAD DUE TO RUDDER AND AILERON ACTIVITY TO KEEP SIDESLIP NEAR ZERO-GIVES IMPRESSION OF LOW DIRECTIONAL STABILITY.
67	7	

### SAILPLANE 3 DATA

TASK	DESCRIPTION OF TASKS	1	2	3	4	5	6	7	AVER. STD DEV
63	B. PILOT OPINION OF CIRCLING FLIGHT	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00
64	1. LOWSPEED HANDLING	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00
65	2. STALL-SPIN SUSCEPTIBILITY	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00
66	3. RISE OF CENTERING THERMAL	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00
67	4. SPEED CONTROL	2.00	2.00	2.00	2.00	2.00	2.00	2.00	2.00
83	AVER. AND STD. DEV. OF SUBTASKS(EX 1,2,...)	1.5	2.0	2.5	3.0	3.5	4.0	4.5	5.0

TASK	PILOT	COMMENTS
0000 0001 0002 0003 0004 0005 0006 0007 0008 0009 0010 0011 0012 0013 0014 0015 0016 0017 0018 0019 0020 0021 0022 0023 0024 0025 0026 0027 0028 0029 0030 0031 0032 0033 0034 0035 0036 0037 0038 0039 0040 0041 0042 0043 0044 0045 0046 0047 0048 0049 0050 0051 0052 0053 0054 0055 0056 0057 0058 0059 0060 0061 0062 0063 0064 0065 0066 0067 0068 0069 0070 0071 0072 0073 0074 0075 0076 0077 0078 0079 0080 0081 0082 0083 0084 0085 0086 0087 0088 0089 0090 0091 0092 0093 0094 0095 0096 0097 0098 0099 0100	UNUSUAL	PLEASANT, ALTHOUGH STICK FORCES ON THE LIGHT SIDE NO STALL-SPIN TENDENCY OBSERVED WHILE THERMALING COMFORTABLE TENDENCY TO PITCH IN TURBULENT THERMALS BITTER THAN SAILPLANE 2 WILL OCCASIONALLY SELF-TIGHTEN DURING STRONG UP-GUSTS. CAN TIGHTEN UP INTO STALL IN STRONG GUST ONE FEELS IMMEDIATELY AT HOME IN THE SHIP GOOD CONTROL HARMONY AT 50KTS BUT POOR AT HIGHER SPEEDS. RUDDER COORDINATION AND AIRSPEED CONTROL CREATE FAIRLY HIGH WORKLOAD.

### SAILPLANE 4 DATA

[illegible]

TASK	PILOT	COMMENTS
6000	W. W. W.	GOOD
6005	W. W. W.	NO UNDESIRABLE CHARACTERISTICS NOTED
6010	W. W. W.	TENDS TO OVERCONTROL WITH RUDDER
6015	W. W. W.	NOT AS GOOD AS SAILPLANE 1
6020	W. W. W.	I DON'T FIND TRIMMER OBJECTIONABLE. WING-ROCK IS BOTHERSOME
6025	W. W. W.	WHENEVER BUFFET ENCOUNTERED IN GUSTY THERMAL
6030	W. W. W.	GUSTS GOOD IN CIRCLING FLIGHT. THOUGH NOT AS GOOD AS SAILPLANE 1
6035	W. W. W.	CAUSE NOSE TO CHANGE ATTITUDE UP AND DOWN THIS TENDENCY
6040	W. W. W.	MUST BE BOUGHT BY PILOT TO MAINTAIN THERMAL LOCATION.
6045	W. W. W.	EXCESSIVE TOP ALTITUDE REQUIRED.

\*\*\*\*\* ZEROS INDICATE NO RATING BY PILOT \*\*\*\*\*

# SAILPLANE 5 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV							
63	B. PILOT OPINION OF CIRCLING FLIGHT	2.50	3.00	1.00	.00	.00	3.00	2.00	2.300	.748							
64	1. LOWSPEED HANDLING	2.00	.00	2.00	.00	.00	3.00	2.00	2.400	.490							
65	2. STALL-SPIN SUSCEPTIBILITY	3.00	.00	2.00	.00	.00	3.00	2.00	2.400	.490							
66	3. EASE OF CENTERING THERMAL	3.00	.00	1.00	.00	.00	2.00	2.00	2.750	1.000							
67	4. SPEED CONTROL	2.00	2.00	1.00	.00	.00	2.00	2.00	2.200	.480							
83	AVER. AND STD. DEV. OF SUBTASKS(EX 1+2+...)	2.0	.7	2.5	.5	1.7	.5	.0	.7	.0	.7	2.7	.8	2.0	1.2	2.2	.89

TASK	PILOT	COMMENTS
63	1	EXCELLENT NOT SUSCEPTIBLE NOT TRIED LOW STICK FORCE/OK RATHER NICE FOR THERMALING, BETTER THAN SMALLER SPAN GLIDERS STICK CANNOT BE RELEASED FOR MORE THAN A FEW SECONDS IN STEEPLY BANKED CIRCLING FLIGHT, FAIRLY LARGE LONG. STICK INPUTS COULD BE MADE WITHOUT ANY CHANGE IN SPEED OR (G) FORCES. (ELASTIC EFFECTS) ROLL RATE AND YAW DUE TO AILERON MAKE THERMAL CENTERING DIFFICULT IN SMALL ROUGH THERMALS. VERY STABLE IN BANK ANGLE BUT ATTENTION REQUIRED TO CONTROL AIRSPEED.

# SAILPLANE 6 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV						
63	B. PILOT OPINION OF CIRCLING FLIGHT	.00	.00	2.00	.00	.00	2.00	3.00	2.333	2.625						
64	1. LOWSPEED HANDLING	.00	2.00	.00	.00	.00	2.00	3.00	2.000	3.162						
65	2. STALL-SPIN SUSCEPTIBILITY	.00	2.00	.00	.00	.00	2.00	3.00	2.333	2.887						
66	3. EASE OF CENTERING THERMAL	.00	2.00	.00	.00	.00	2.00	3.00	2.333	2.887						
67	4. SPEED CONTROL	.00	2.00	.00	.00	.00	2.00	3.00	2.333	1.247						
83	AVER. AND STD. DEV. OF SUBTASKS(EX 1+2+...)	.0	.0	4.0	.7	.0	.0	.0	.0	.0	6.7	1.9	2.7	.4	4.5	2.06

TASK	PILOT	COMMENTS
63	1	GOOD EXCEPT NEAR STALL GOOD, BUFFETING IS ANNOYING MODERATE BREAKS OFF INTO INCIPIENT SPIN EASILY YES GOOD EXCESSIVE PITCH FORCE CHANGE WITH BANK CHANGE EXCELLENT, BUT ON HEAVY SIDE HIGH WORKLOAD! TURBULENCE CAUSES UPSETS IN ALL THREE AXES, REQUIRING LOTS OF STICK AND RUDDER MOVEMENT

\*\*\*\*\* ZEROS INDICATE NO RATING BY PILOT \*\*\*\*\*

#### SAILPLANE 1 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV
68	C. PILOT OPINION OF CRUISING FLIGHT	1.00	1.00	1.00	2.00	2.00	2.00	1.00	1.600	1.200
69	1. EASE OF CONTROLLING AIRSPEED	1.00	1.00	1.00	2.00	2.00	2.00	1.00	1.667	1.155
70	2. PULL UP INTO THERMAL	1.00	1.00	1.00	2.00	2.00	2.00	1.00	1.667	1.155
71	3. EASE OF PERF. SECONDARY TASKS	1.00	1.00	1.00	2.00	2.00	2.00	1.00	1.667	1.155
72	4. RIDE QUALITY	1.00	1.00	1.00	2.00	2.00	2.00	1.00	1.667	1.155
73	5. EASE OF MAIN. STRAIGHT FLIGHT	1.00	1.00	1.00	2.00	2.00	2.00	1.00	1.667	1.155
64	AVER. AND STD. DEV. OF SUBTASKS(EX 1:2,..)	1.0	1.0	1.4	1.5	1.8	1.2	1.0	1.7	.79

TASK	PILOT	COMMENTS
69	5	BELOW 61IAS--3 ABOVE 61IAS DUE TO TRIM
69	5	UNABLE TO TRIM TO HIGH SPEEDS, I.C. ABOVE 61KTS.
70	5	SPEED BLEEDS OFF QUICKLY, HAVE TO WATCH IT.
71	5	EXCELLENT
72	5	GOOD, BUT SMALL, UNCOMFORTABLE COCKPIT DEGRADES IT
73	5	EXCELLENT
64	5	LARGE ATTITUDE CHANGES WITH AIRSPEED
64	5	VERY LOW WORKLOAD, OVERALL, THE BEST FLYING OF ALL SAILPLANES
64	5	THEY SHOULD ALL FLY THIS WAY!

#### SAILPLANE 2 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV
68	C. PILOT OPINION OF CRUISING FLIGHT	1.00	2.00	2.00	2.00	2.00	2.00	2.00	2.200	.980
69	1. EASE OF CONTROLLING AIRSPEED	1.00	2.00	2.00	2.00	2.00	2.00	2.00	2.167	.987
70	2. PULL UP INTO THERMAL	1.00	2.00	2.00	2.00	2.00	2.00	2.00	2.167	.987
71	3. EASE OF PERF. SECONDARY TASKS	1.00	2.00	2.00	2.00	2.00	2.00	2.00	2.167	.987
72	4. RIDE QUALITY	1.00	2.00	2.00	2.00	2.00	2.00	2.00	2.167	.987
73	5. EASE OF MAIN. STRAIGHT FLIGHT	1.00	2.00	2.00	2.00	2.00	2.00	2.00	2.167	.987
64	AVER. AND STD. DEV. OF SUBTASKS(EX 1:2,..)	1.2	1.4	1.5	2.0	2.0	2.0	2.0	2.2	.96

TASK	PILOT	COMMENTS
70	5	VERY PLEASANT
71	5	DIFFICULT
72	5	GOOD
73	5	NO PROBLEM
73	5	DIRECTIONALLY LOOSE
73	5	NOSE WANDERS, BUT NOT SO AS TO DETRACT FROM MISSION
64	5	POUNCE BECAUSE OF WING FLEXING.
64	5	VERY EASY TO CHANGE SPEEDS. NEGATIVE FLAPS RESULT IN QUICK AIRSPEED
64	5	CHANGES(QUICKER THAN SAILPLANE 5) WITH NO ATTITUDE OR SOUND CHANGES.
64	5	THIS FEATURE MAY MAKE SHIP DIFFICULT FOR TRANSITIONING.



\*\*\*\*\* ZEROS INDICATE NO RATING BY PILOT \*\*\*\*\*

#### SAILPLANE 3 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV							
68	C. PILOT OPINION OF CRUISING FLIGHT	1.50	3.00	3.50	.00	.00	4.00	3.00	2.600	.970							
69	1. EASE OF CONTROLLING AIRSPEED	.00	3.00	3.50	.00	.00	4.00	3.00	2.333	.943							
70	2. PULL UP INTO THERMAL	.00	3.00	3.50	.00	.00	4.00	3.00	2.333	.943							
71	3. EASE OF PERFF. SECONDARY TASKS	.00	3.00	3.50	.00	.00	4.00	3.00	2.333	.943							
72	4. RIDE QUALITY	.00	3.00	3.50	.00	.00	4.00	3.00	2.333	.943							
73	5. EASE OF MAIN, STRAIGHT FLIGHT	1.00	1.00	1.00	.00	.00	4.00	3.00	1.500	.500							
84	AVER. AND STD. DEV. OF SUBTASKS(EX 1,2,...)	1.6	.5	2.6	1.0	1.3	.4	.0	.0	2.8	.7	2.6	.8	2.4	.5	2.2	.89

TASK	PILOT	COMMENTS
68	3	EASY TASK
69	3	UNABLE TO TRIM TO INTERTHERMAL SPEEDS, I.E. ABOVE 80 KTS.
70	3	FEELS PLEASANT
71	3	OR
72	3	NO HANDS OFF, OVERCONTROLS
73	3	MUST HOLD STICK AT ALL TIMES
74	3	PLEASANT TO FLY
75	3	ANY DISTURBANCE IN PITCH REQUIRES IMMEDIATE ATTENTION
76	3	1,3,4 TENDENCY TO PITCH IN TURBULENT AIR-CAN'T RELEASE STICK
77	3	WITHOUT DIVERGENCE WHETHER CIRCLING OR STRT AND LEVEL FLIGHT.
78	3	FAIRLY LARGE ATTITUDE CHANGES WITH AIRSPEED CHANGE. SAILPLANE 2 IS
79	3	BETTER IN THIS PHASE OF FLIGHT.
80	3	GENERALLY GOOD! POOR CONTROL HARMONY AT HIGHER SPEEDS(SENSITIVE
81	3	PITCH, SLUGGISH AILERONS).

#### SAILPLANE 4 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV						
68	C. PILOT OPINION OF CRUISING FLIGHT	.00	2.00	3.50	.00	.00	2.00	2.00	2.375	.650						
69	1. EASE OF CONTROLLING AIRSPEED	.00	2.00	3.50	.00	.00	2.00	2.00	2.375	.650						
70	2. PULL UP INTO THERMAL	.00	2.00	3.50	.00	.00	2.00	2.00	2.375	.650						
71	3. EASE OF PERF. SECONDARY TASKS	.00	2.00	3.50	.00	.00	2.00	2.00	2.375	.650						
72	4. RIDE QUALITY	.00	2.00	3.50	.00	.00	2.00	2.00	2.375	.650						
73	5. EASE OF MAIN, STRAIGHT FLIGHT	.00	1.00	2.00	.00	.00	2.00	2.00	1.750	.433						
84	AVER. AND STD. DEV. OF SUBTASKS(EX 1,2,...)	.0	.0	1.8	.4	3.0	.5	.0	.0	.0	2.8	.7	2.2	.4	2.4	.72

TASK	PILOT	COMMENTS
68	3	WORKING AGAINST SPRING IS ANNOYING
69	3	WORKING AGAINST SPRING IS ANNOYING
70	3	OCCASIONAL LACK OF COORDINATION NOTED WHILE WATCHING OTHER GLIDERS
71	3	NOISIER THAN MOST
72	3	GOOD
73	3	MAINLY CONCERNED WITH WORKING AGAINST THE FEEL SPRING
74	3	PULL UP TENDS TO PITCH UP TOO HIGH. ROLL AT TOP OK, BUT IF YOU
75	3	OVERSHOOT, UNBANKING MAY BE DIFFICULT DUE TO LACK OF TOP AILERON
76	3	AT SPEEDS BELOW 40 KTS WITH FLAPS AT 314RAD,
77	3	HOLDS HEADING AND SPEED WELL! SECONDARY TASKS CAN BE ATTENDED TO.

\*\*\*\*\* ZEROS INDICATE (0) RATING BY PILOT \*\*\*\*\*

# SAILPLANE 5 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV
68	C. PILOT OPINION OF CRUISING FLIGHT	.00	.00	1.00	.00	.00	3.00	3.00	2.200	.000
69	1. EASE OF CONTROLLING AIRSPEED	.00	.00	1.00	.00	.00	5.00	3.00	2.400	1.356
70	2. PULL UP INTO THERMAL	.00	.00	1.00	.00	.00	2.00	2.00	2.000	.632
71	3. EASE OF PERF. SECONDARY TASKS	.00	.00	1.00	.00	.00	4.00	4.00	3.200	1.939
72	4. RIDE QUALITY	.00	.00	1.00	.00	.00	2.00	3.00	1.800	.740
73	5. EASE OF MAIN. STRAIGHT FLIGHT	.00	.00	1.00	.00	.00	3.00	2.00	1.400	.000
84	AVER. AND STD. DEV. OF SUBTASKS(EX 1:2+...)	1.2	.4	2.8	1.7	1.2	.4	.0	.0	1.34

TASK	PILOT	COMMENTS
69	6	AT HIGH CRUISING SPEEDS, UNABLE TO TRIM. POSITIVE [RE] GIVES NOSE UP
69	6	INPUT TO STICK
70	6	SPECTACULAR DUE TO LARGER KINETIC ENERGY OF GLIDER
71	6	MUST HOLD STICK RIGID, NOT UNPLEASANT IF CONTROL TASK IS VERY
71	6	OPEN LOOPS.
72	6	OK
73	6	EXCELLENT
73	6	EXCELLENT
73	6	CAN'T LET GO OF STICK
84	6	IN TURBULENCE, IN THE APPROACH CONFIGURATION, FULL PILOT ATTENTION
84	6	IS REQUIRED. SLOWER ROLL RATE IS NOTICEABLE. LOT OF RUDDER ACTIVITY
84	6	WAS NEEDED IN THIS PHASE OF FLIGHT.
84	6	AT 85-90 KTS PENETRATION SPEED, QUIET EXCEPT FOR LIGHT RATTLE IN
84	6	WINGS! ATTENTION TO AIRSPEED(PITCH) CONTROL LEAVES LITTLE TIME FOR
85	6	SECONDARY TASKS! TURBULENCE CAUSES CONTINUAL SMALL PITCH UPSETS.

# SAILPLANE 6 DATA

TASK	DESCRIPTION OF TASKS	1	2	PILOT 3	4	5	6	7	AVER.	STD DEV
68	C. PILOT OPINION OF CRUISING FLIGHT	.00	.00	1.00	.00	.00	2.00	2.00	1.667	.471
69	1. EASE OF CONTROLLING AIRSPEED	.00	.00	1.00	.00	.00	2.00	2.00	1.500	.500
70	2. PULL UP INTO THERMAL	.00	.00	1.00	.00	.00	2.00	2.00	1.500	.500
71	3. EASE OF PERF. SECONDARY TASKS	.00	.00	1.00	.00	.00	2.00	2.00	1.500	.500
72	4. RIDE QUALITY	.00	.00	1.00	.00	.00	2.00	2.00	1.500	.500
73	5. EASE OF MAIN. STRAIGHT FLIGHT	.00	1.00	2.00	.00	.00	2.00	2.00	1.750	.433
84	AVER. AND STD. DEV. OF SUBTASKS(EX 1:2+...)	.0	.0	1.2	.4	1.8	.7	.0	.0	.92

TASK	PILOT	COMMENTS
69	6	EXCELLENT
70	6	SHOULD BE VERY MODERATE IN THIS GLIDER
71	6	AIRSPEED DECREASES VERY RAPIDLY
72	6	QUICK, EASY BECAUSE OF LARGE STABILITY
73	6	NOT AS SOFT AS GLASS SHIP, NOISY
73	6	GOOD
84	6	LARGE ATTITUDE CHANGES WITH AIRSPEED, NOISY AT TIMES
84	6	SAME GENERAL COMMENTS AS FOR CIRCLING FLIGHT

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16. Abstract <p>Seven test pilots flew six sailplanes in a round-robin evaluation of sailplane handling qualities. An evaluation was made of the handling qualities over the sailplane operational envelope using the Cooper-Harper Rating Scale and pilot comments as the evaluation instrument. The sailplanes were chosen to represent the range of handling and performance characteristics of high performance sailplanes in current use.</p> <p>The evaluation sailplanes were found generally deficient in the area of cockpit layout. The pilots indicated general dissatisfaction with high pitch sensitivity especially when coupled with inertially induced stick forces. While all sailplanes were judged satisfactory for centering thermals and in the ease of speed control in circling flight, pilot opinions diverged on the maneuvering response, pull-out characteristics from a dive, and on phugoid damping. Lateral-directional control problems were noted mainly during takeoff and landing for most sailplanes with the landing wheel ahead of center of gravity. Pilot opinion of in-flight lateral-directional stability and control was generally satisfactory. Five of the evaluation sailplanes exhibited a very narrow airspeed band in which perceptible stall warning buffet occurred. However, this characteristic was considered not objectionable when stall recovery was easy. The pilots objected to the characteristics of a wide airspeed band of stall warning followed by a stall with yawing and rolling tendency and substantial loss of altitude during the stall. Glide path control for the evaluation sailplanes was found to be generally objectionable.</p>					
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